Soft Protection Approaches Beach nourishments, dune rehabilitation and

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eco-engineering

Jaap van Thiel de Vries



Challenge the future

Delft University of Technology

TUDelft

Program

• Part I: Approaches and Technology (9:00-11:00)

- Causes of coastal erosion
- Soft protection approaches
- Nourishments: The Dutch approach
- Building with Nature
- Mega nourishments: The Sand Engine
- Part II: Modelling event driven erosion (XBeach) (11:00-16:00)
 - Event driven erosion
 - XBeach Model concept
 - Hand on: Evaluate nourishment strategy at Kijkduin (NL) / hurricane case SantaRosa island
 - Advanced functionality: dune revetments, coral reefs, vegetation, gravel, long term simulations
- Part III: Presentation of local problems (by participants) (16:00-18:00)
 - Let participants prepare a few (=2) slides about there case







Part

Causes of coastal erosion







Types of coastal erosion processes Two types of erosion

1. Structural erosion

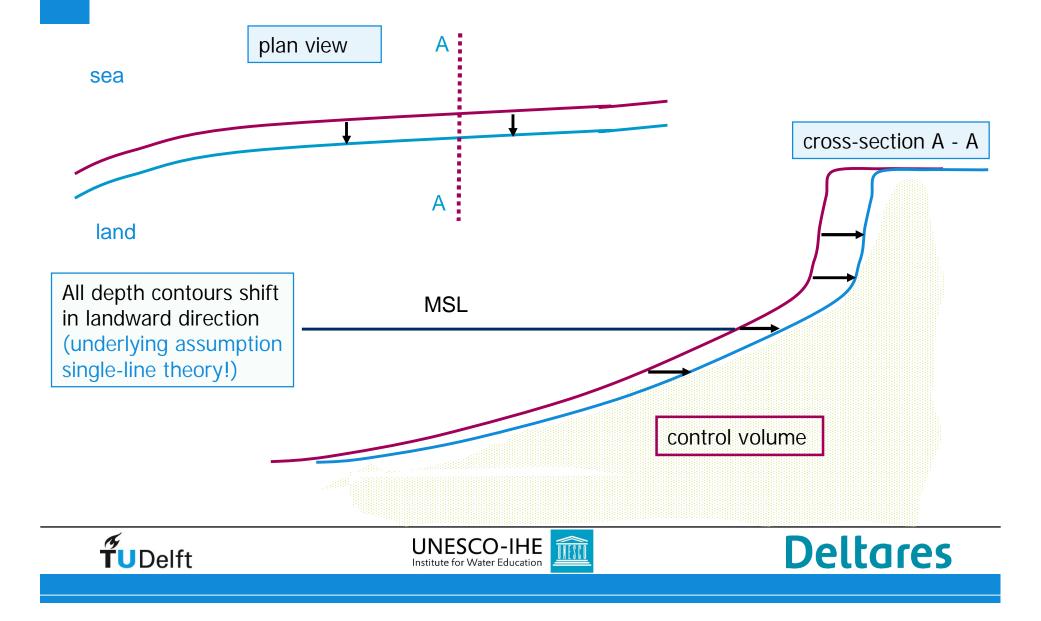
- long-term, gradual, due to 'normal' and slow processes
- e.g. 1 m/yr or 20 m³/m per year (if profile height is 20 m)
- 2. Episodic erosion, during severe storm (surge) events
 - i.e. dune erosion due to storm surge
 - fast process (hours)
 - e.g. 100 m³/m in 6 hours or even 200 to 300 m³/m (10 15 m) under design conditions

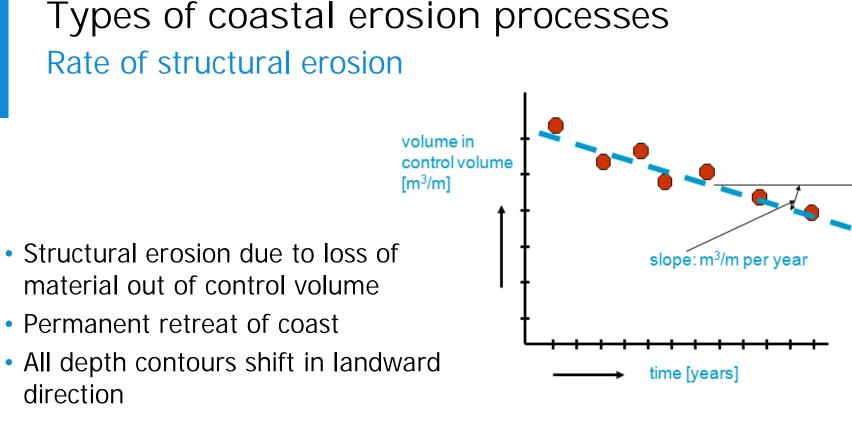






Types of coastal erosion processes Structural erosion – control volume





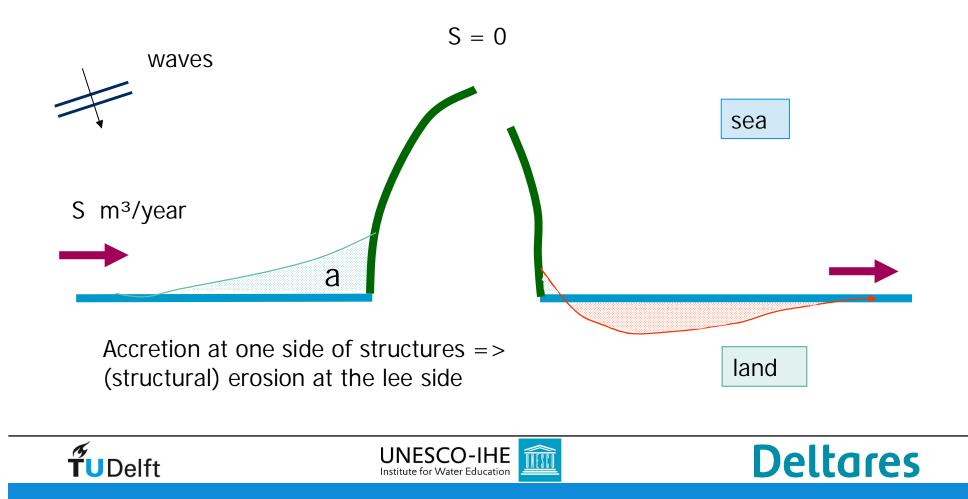
 Structural erosion is often caused by gradient in longshore sediment transport







Types of coastal erosion processes Example of structural erosion - Port



Types of coastal erosion processes Dune erosion (episodic erosion)

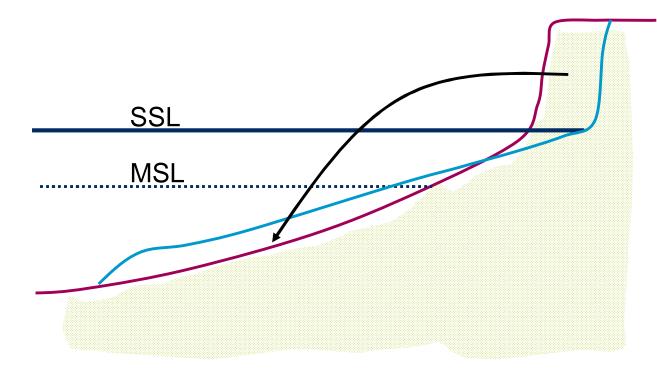








Types of coastal erosion processes Episodic erosion (dune erosion)



- storm event (SSL)
- redistribution over cross-shore profile
- no loss out of control volume
- return of sediments in non-storm season (in stable situations, i.e. no structural erosion)







Cyclic profile and bar behaviour

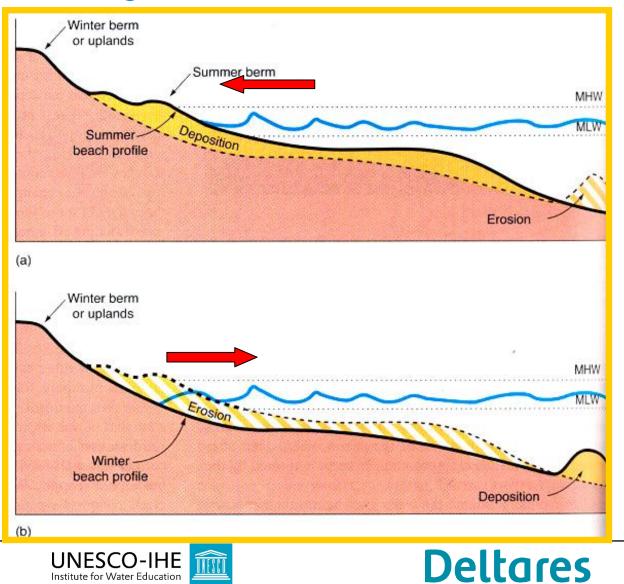
Storm and seasonal changes

Summer: beach rich in sediment (resembling reflective beach)

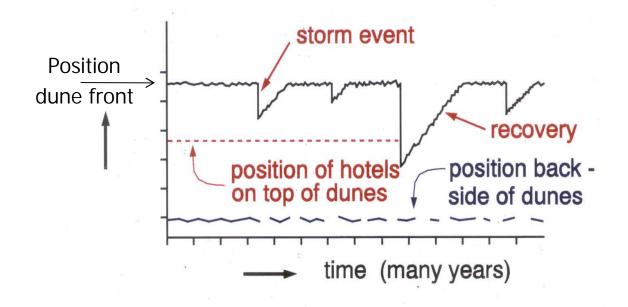
Winter and/or after storm: beach poor in sediment

(resembling dissipative beach)

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Types of coastal erosion processes Episodic erosion along a stable coast



Stable coast + storm surge events







Part I

Artificial Nourishments







Coastal protection strategies

Selection of coastal protection method

- Important to have good insight in coastal processes
- Two basic approaches:
 - 1. Try to solve the cause of the erosion problem (cure the cause)
 - 2. Mitigate the negative effects (cure the symptoms)
- Possible solutions to mitigate coastal erosion problems:
 - "soft" (natural) measures (beach and foreshore nourishment)











Coastal protection strategies Selection of coastal protection method

"Soft" methods: beach or foreshore nourishment

- Principle: compensate for eroded sand
- Erosion process does continue
- Must be repeated on regular basis
- If possible use sand from maintenance dredging ("make work with work")

Special "Soft" method: by-pass systems

 Re-store sediment transports from up-drift side of structure to down-drift side in an artificial way (pumping)











Coastal protection strategies

Selection of coastal protection method

"Hard" methods: groynes, offshore breakwaters, revetments, seawalls

- Principle = reduce erosion by interfering in sediment transports both alongshore and cross-shore
- But causes impact on down-drift coast!

Sub-division of "hard" methods

- Structures influencing longshore transport under both normal and extreme conditions (groynes, dam, detached breakwaters);
- Structures preventing erosion during extreme storm events (sea wall, revetment, sea dike).





Deltares





Artificial nourishment ('soft' measures) Introduction

- Artificial sand nourishment to:
 - Compensate structural erosion (regular basis).
 - Protect beach and dunes against storm erosion.



- Create new beaches or reclaim new land.
- Must be repeated regularly (only treating symptoms).
- Leaves coast in natural state, without lee-side erosion.
- Flexible: scheme can be modified if results are not as expected.
- Good for coastal system: sediment is added to it.







Artificial nourishment ('soft' measures) Introduction

- Nourishment can "never" go wrong (except for bad designed nourishment scheme, leading to damage of properties)
- Often economic solution due to its cost structure (no capital cost, only maintenance cost).



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Design aspects - Origin of sand

Borrow sand

- Land sources (river beds or sand deposits)
- Marine sources (estuaries or sea bed)
- Maintenance dredging (Dutch: "werk met werk maken")

Borrow pit

- At sufficiently large distance from shore (in NL = 20 km) to prevent erosion;
- Small and deep versus large and shallow?
 - Deep => stagnant water with poor quality
 - Large => environmental disturbance of surface layer
 - No clear recommendation. Perform environmental study









Artificial nourishment ('soft' measures) Design aspects - Quality of sand

- Use preferably borrow sand that is similar to native material (same behavior)
- Sometimes coarser material is used to reduce losses (steeper slopes).
- Borrow material contains silt (2% is normal), which may have negative impact on marine environment (during overflow).
- If necessary wash out silt before placing sand on beach.



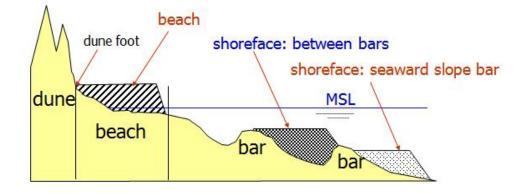






Artificial nourishment ('soft' measures) Design aspects - Location of nourishment

- Location of nourishment:
 - Landward slope of dunes
 - Seaward slope of dunes
 - Dry beach
 - Shoreface



- Sand for (landward) dune nourishment is often from land sources, because marine sand may cause salt problems for dune vegetation.
- Placing sand on beach requires dredging equipment to cross breaker zone. Rainbowing is alternative solution (shallow water).







Artificial nourishment ('soft' measures) Design aspects - Location of nourishment

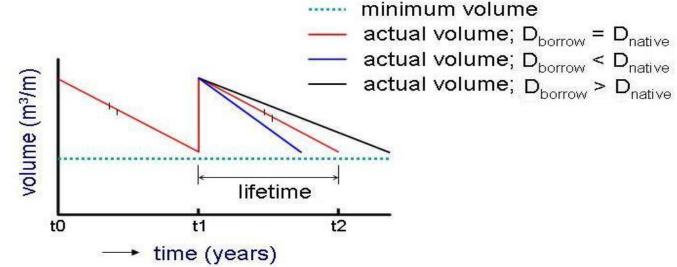
- Shoreface nourishments are placed at the seaward edge of the surf zone where navigational depth of hopper dredger is sufficient.
- Shoreface nourishment may be more economical and recreationfriendly than beach nourishments.
- Effectiveness of beach nourishment is higher, but for higher unit cost.







Re-nourishment for structural erosion



- Start re-nourishment at moment of minimum beach volume (t_1) .
- Generally lifetime is 5 to 10 years (due to high mobilization costs).
- If borrow and native sand is the same => erosion is the same (red) = > lifetime is $(t_2 - t_1) = (t_1 - t_0)$.
- Borrow sand coarser => loss decreases => lifetime increases (black)
- Borrow sand finer => loss increases => lifetime decreases (blue)







Example nourishment project

Assume coastline retreat is 2 m per year
 => sand loss over total profile height
 (20 m) is ΔV = 40 m³/m' per year.



- Assume period between nourishments is
 5 year => volume to be nourished is 200 m³/m' every 5 years.
- Assume stretch of coast is 5 km long => total volume to be nourished is 1,000,000 m³ every 5 years.
- Volume is increased with 10% to 20% to account for additional losses of the fine fraction.
- Make "win-win" contract with contractor:
 - Long term contract
 - Control method (as built survey or hopper volume measurements)
 - Combine foreshore with beach nourishment (flexibility contractor).







Shoreface nourishment

 Nourishment volume in order of 300 to 500 m³/m' over alongshore distance of 2 to 5 km.



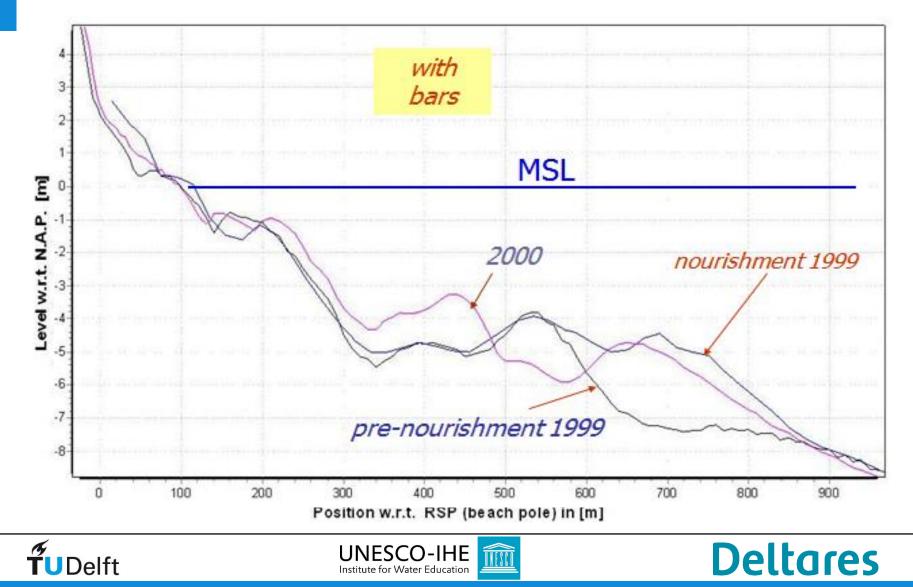
- Larger nourishment volumes are required as only 30% to 50% of nourishment volume will reach beach zone.
- Shoreface nourishments add large volumes of sand to the system.
- Costs per m³ for shoreface nourishment are 50% to 70% less than for beach nourishment (total cost in balance?!).
- Large shoreface nourishments impact sediment transport processes (may behave like submerged breakwater, although effect diminishes in time).





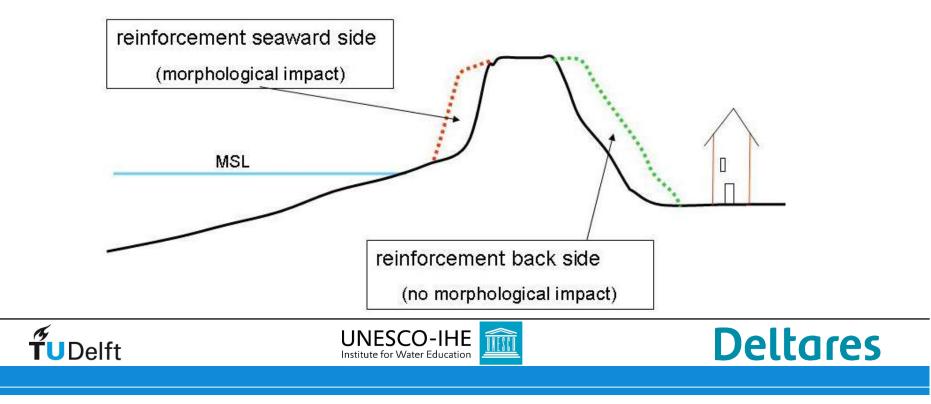


Shore face nourishment: movement of sand towards beach



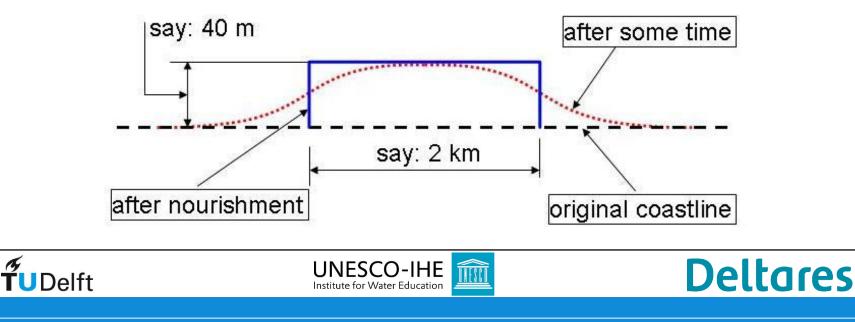
Artificial nourishment ('soft' measures) Dune nourishment

- Dune nourishment required if volume of dune is insufficient to cope with dune erosion during design storm.
- Nourishment at landward side is most effective (infrastructure?)
- Nourishment at seaward side or on top of dune interferes with the coastal dynamic system (effective but sand may be "lost" for dune)



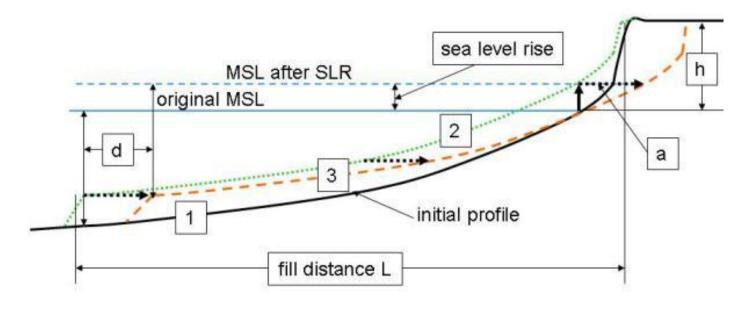
Artificial nourishment ('soft' measures) Dune nourishment: two options

- Landward side
 - Most effective, but may be not possible due to presence of infrastructure and properties.
- Seaward side
 - Relatively large volume of sand is required to account for redistribution of the sand over the cross-shore profile, due to morphological impact.
 - So local dune reinforcement will have a relatively short life-time.



Nourishment to counteract sea-level rise

- Nourishments fills in space between profile 1 and 2 created by the sea-level rise Required volume is *SLR* x distance *L*
- E.g. SLR = 1.0 m per century and L = 1000 m, a volume of 1000 m³/m is required in 100 yrs => 10 m³/m per yr.
- 100 m³/m per 10 year nourishment interval is usual number.



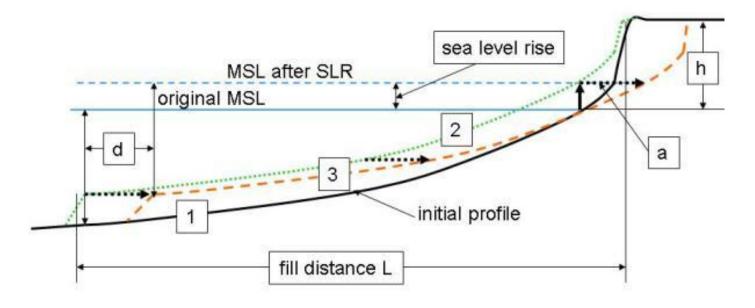
Deltares





Artificial nourishment ('soft' measures) If no nourishment is used to counteract sea-level rise?

- Without nourishment profile 3 is equilibrium coastal profile (see Chapter 7).
- Profile 3 is obtained by horizontal shift of profile 2 over distance a.
- $a = (SLR \times L)/(d + h) = (1 \text{ m}/100 \text{ yr} \times 1000 \text{ m})/(10 \text{ m} + 10 \text{ m}) = 0.5 \text{ m/yr}$
- Result is structural coastal erosion!



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Artificial nourishment ('soft' measures) Land reclamation

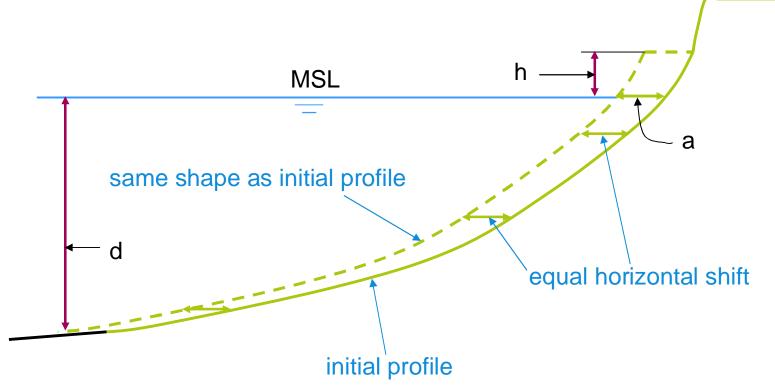








Artificial nourishment ('soft' measures) Land reclamation

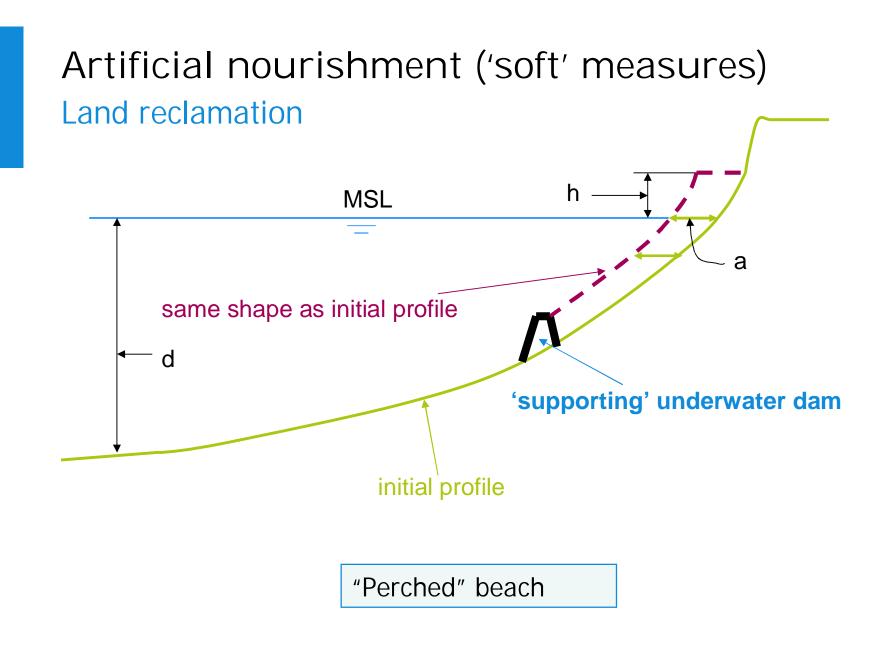


 $d = 15 \text{ m}; \text{ } \text{h} = 10 \text{ } \text{m} \text{ ---> } 1 \text{ } \text{m}^2 \text{ of 'new' land: } 25 \text{ } \text{m}^3; \text{ costs?}$







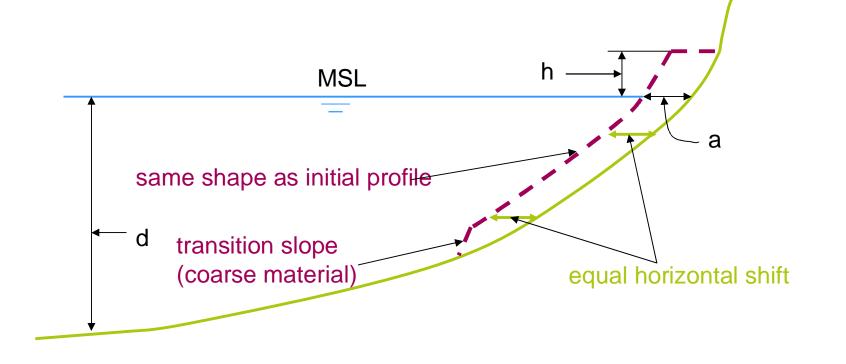








Artificial nourishment ('soft' measures) Land reclamation



Other methods?







Part 1

The Dutch approach







The Dutch coast

- 1. Wadden
- 2. Holland
- 3. Delta











Coastal protection strategies

Coastal zone management strategies

Why?

- Increased pressures on coastal zone
- Changing conditions (climate, SLR)

CZM strategies:

- Retreat (simple solutions in future?)
- Accommodate (adapt infrastructure)
- Protect (take measures)

Important to define proper CZM strategy, taking into account use of the coastal zone (social, economic and cultural) in relation to the cost for protection (Chapter 11).

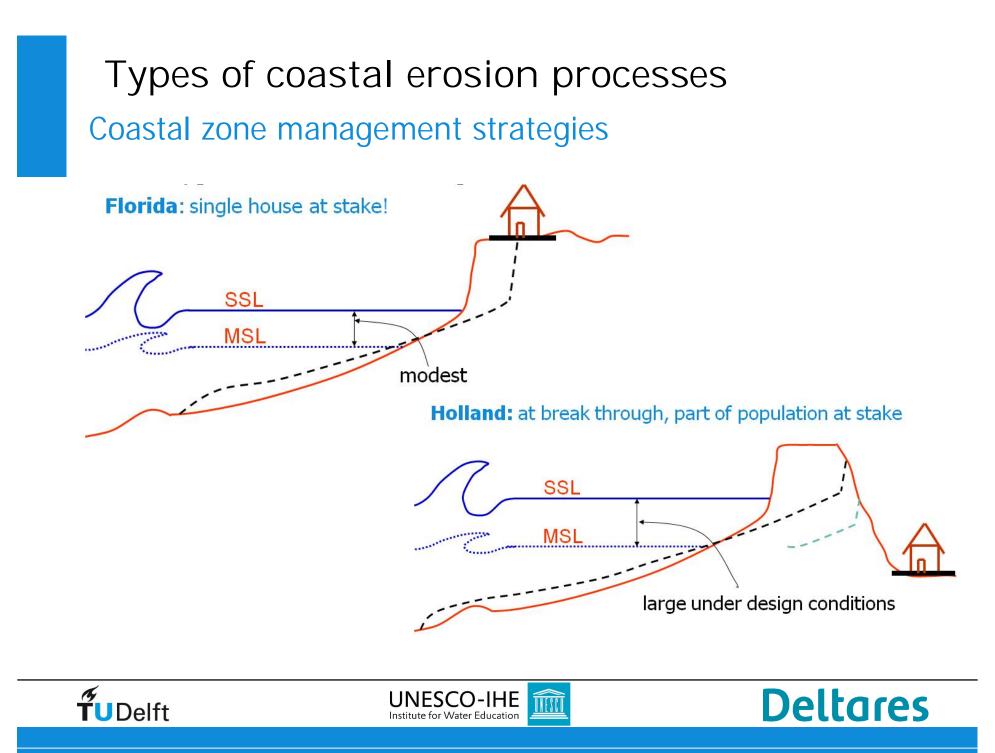
This lecture only deals with "Protect".











Coastal protection strategies

Coastal zone management strategies

Actual Coastal Protection Strategy of Rijkswaterstaat (Dutch Ministry of Infrastructure and Environment)

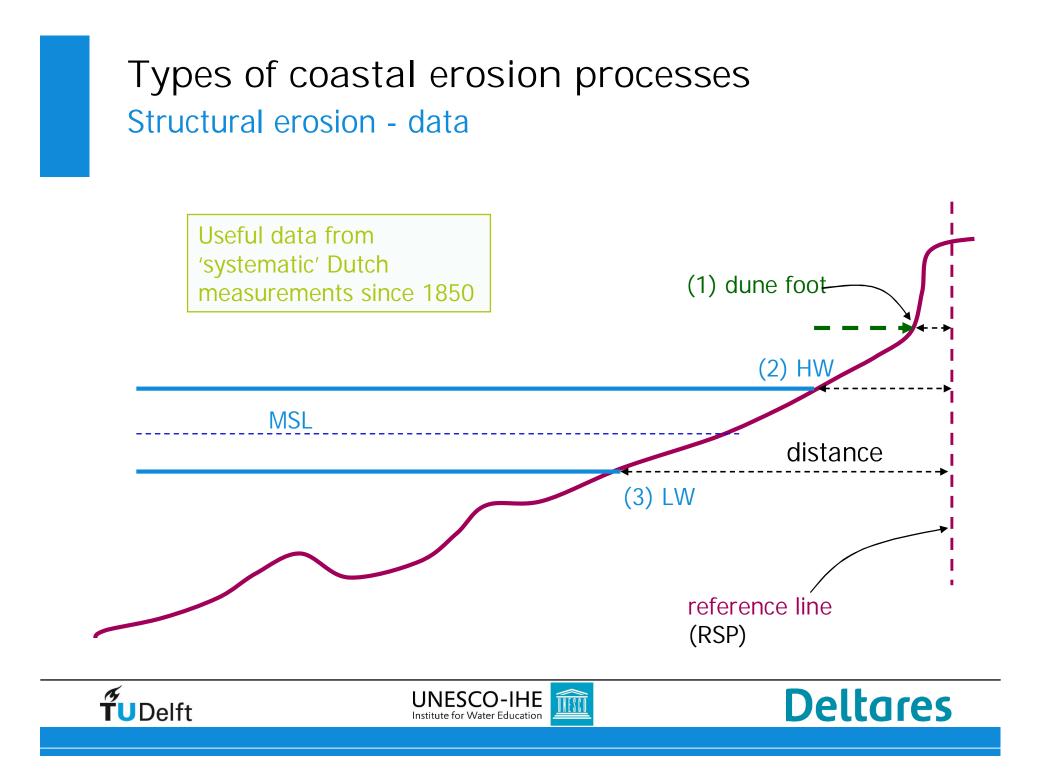
• "Soft" if possible, "hard" if required.

• Nourishment at foreshore if possible, at beach if required.

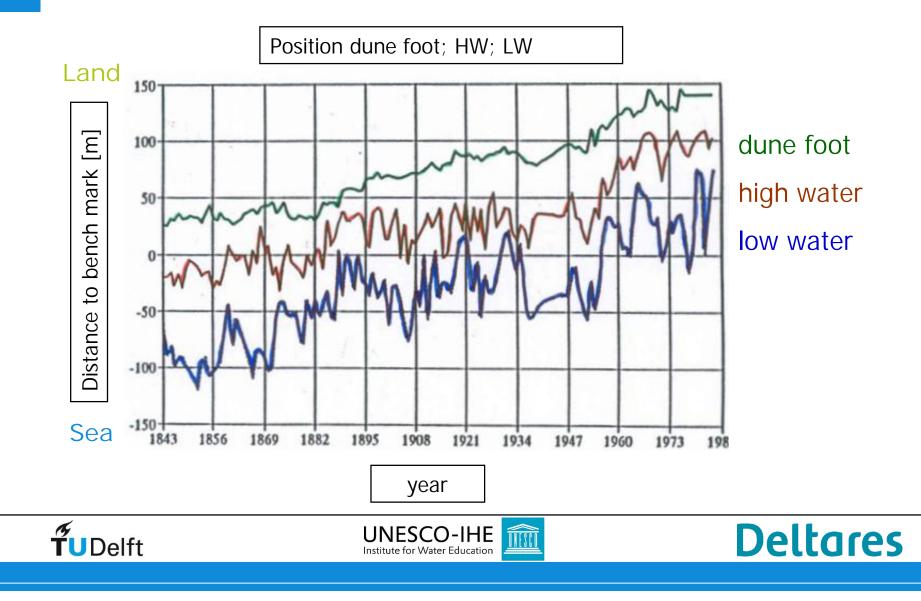


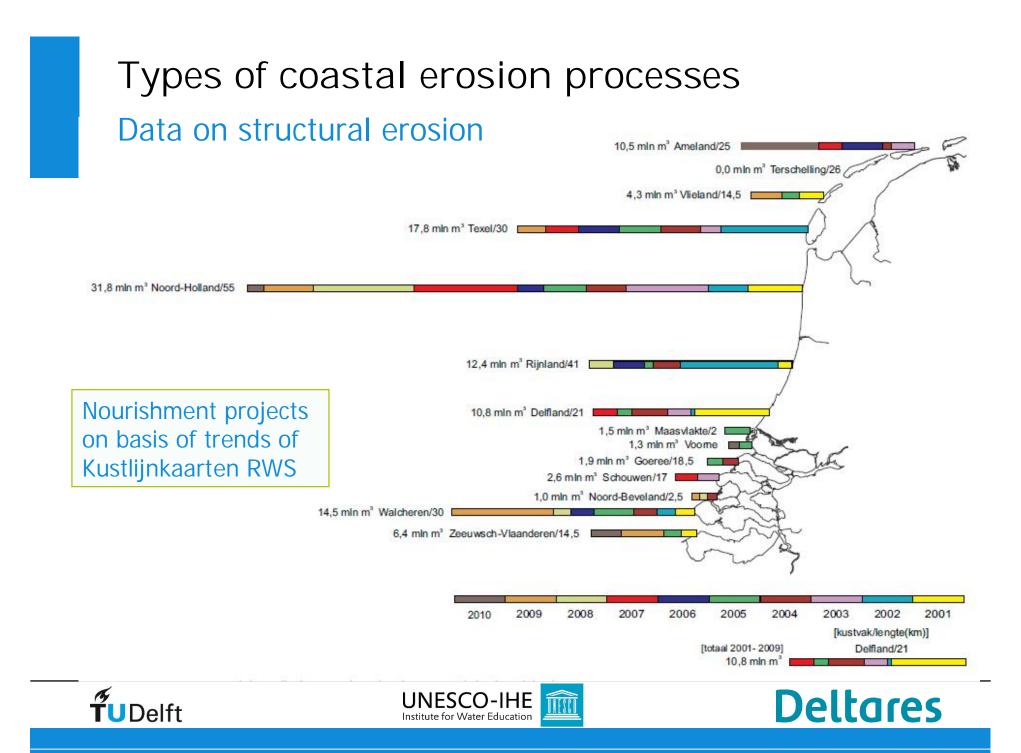






Types of coastal erosion processes Structural erosion – data ("lightning graphs")





Types of coastal erosion processes

Data on structural erosion. RWS "Kustlijnkaarten 2011"



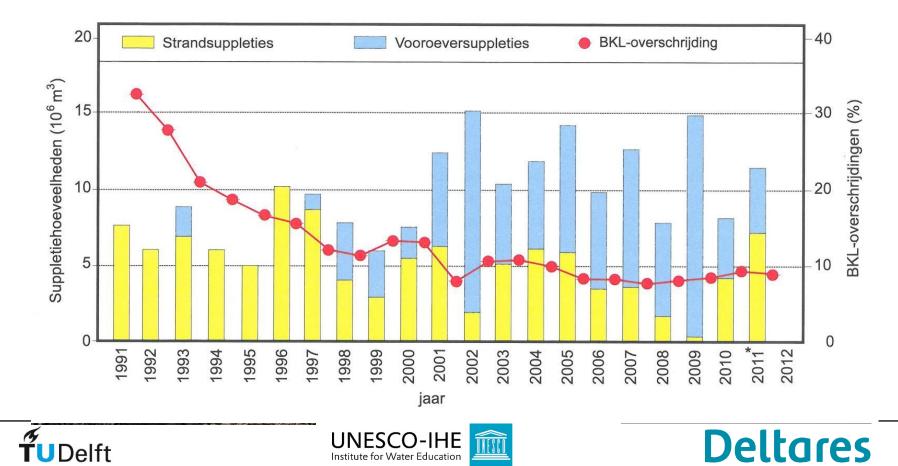






Results of 20 years of nourishing





Part 1

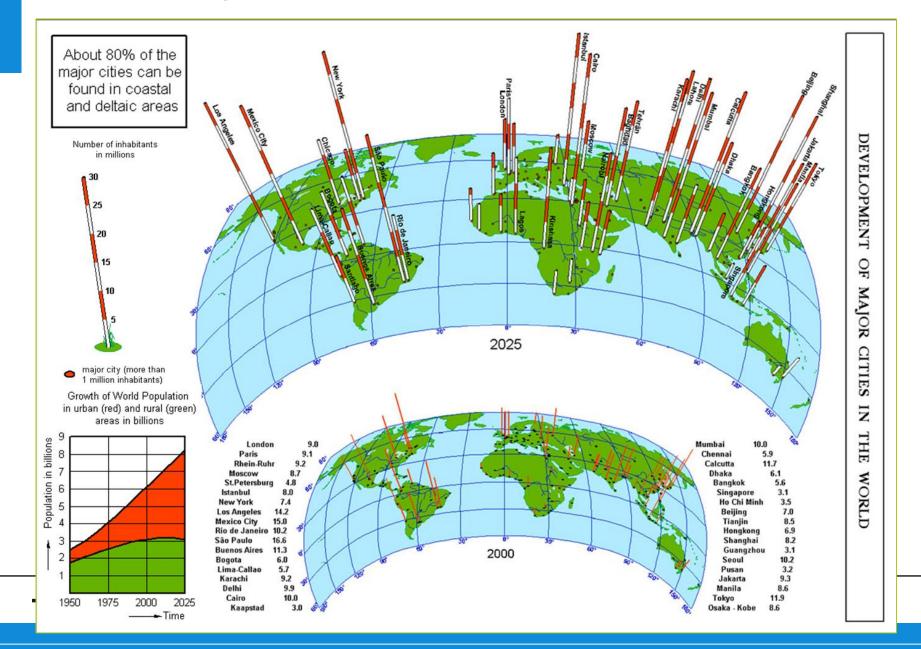
Building with Nature







Increasing pressure on deltas worldwide



Global trade growth



Container and bulk transport boost the need for port capacity





UNESCO-II Institute for Water Educ

Global energy consumption



Oil & Gas trade flows generate LNG and Offshore pipeline projects

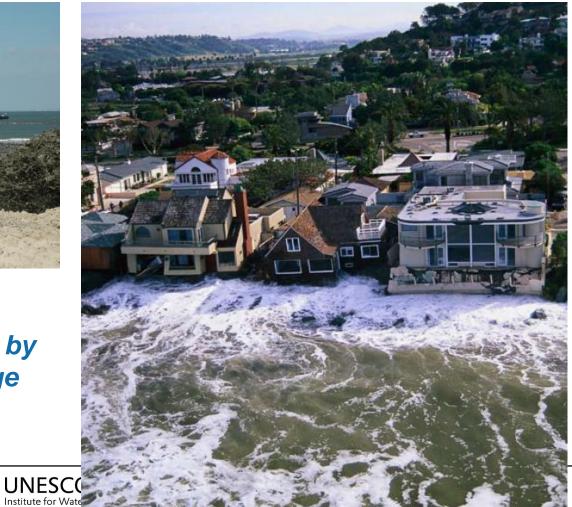




Climate change



Pressures are reinforced by effects of climate change







Ongoing need for marine infrastructure development

... while at the same time ...

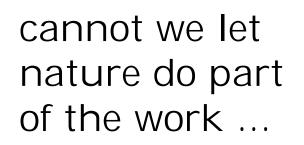
Increasing environmental awareness



Is what we do truly sustainable ???



Building with Nature



while creating new new opportunities for itself?

young dune formation



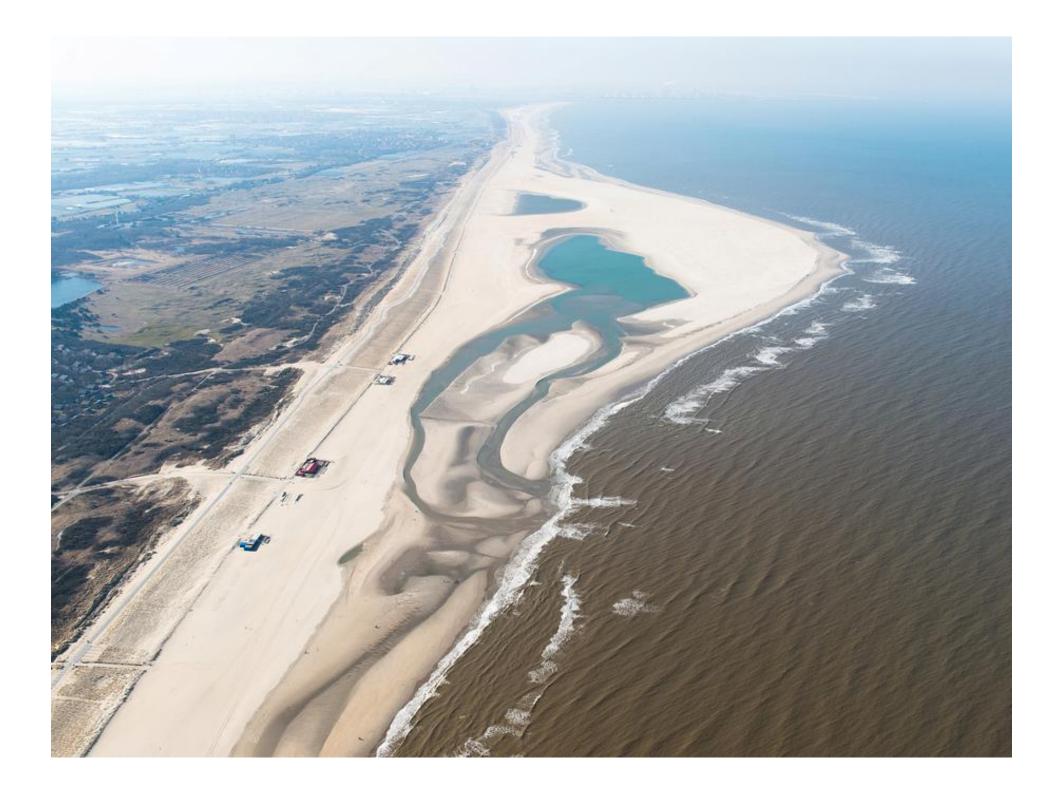
new ties

Building with Nature solutions

soft solutions

hard solutions





The Dutch coast

- 1. Wadden
- 2. Holland
- 3. Delta









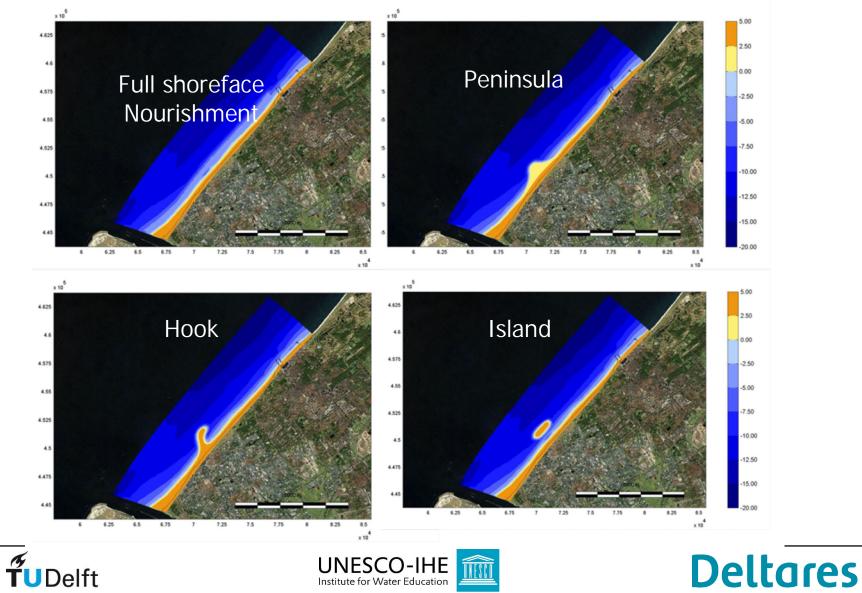






(and profit at the same time)

Design alternatives

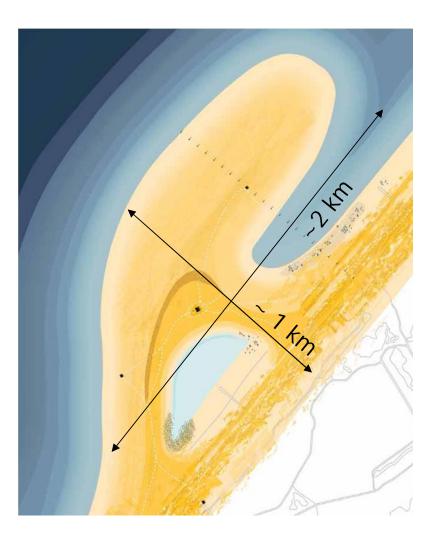


Design

Objectives: 1.Extra Safety 2.Nature area / 'Quality of living' 3.Innovation

'Hook' altenative

70 M Euro. 21 M m³ of sand









Expected advantages

enhanced safety against flooding

(first: wave attenuator; later: wider dune buffer)
cheaper per m3 compared to traditional nourishments
(but: costs brought forward → interest!)
longer period between consecutive nourishments
more time for beach and shoreface ecosystem to recover
ecologically interesting intermediate stages
beach lagoons, juvenile dunes, pioneer vegetation

recreation potential

swimming, surfing, beach recreation

wider dune area

increased freshwater reserve

Construction

Suction hopper:

- Pumping ashore
- Bottom dumping
- Rainbowing





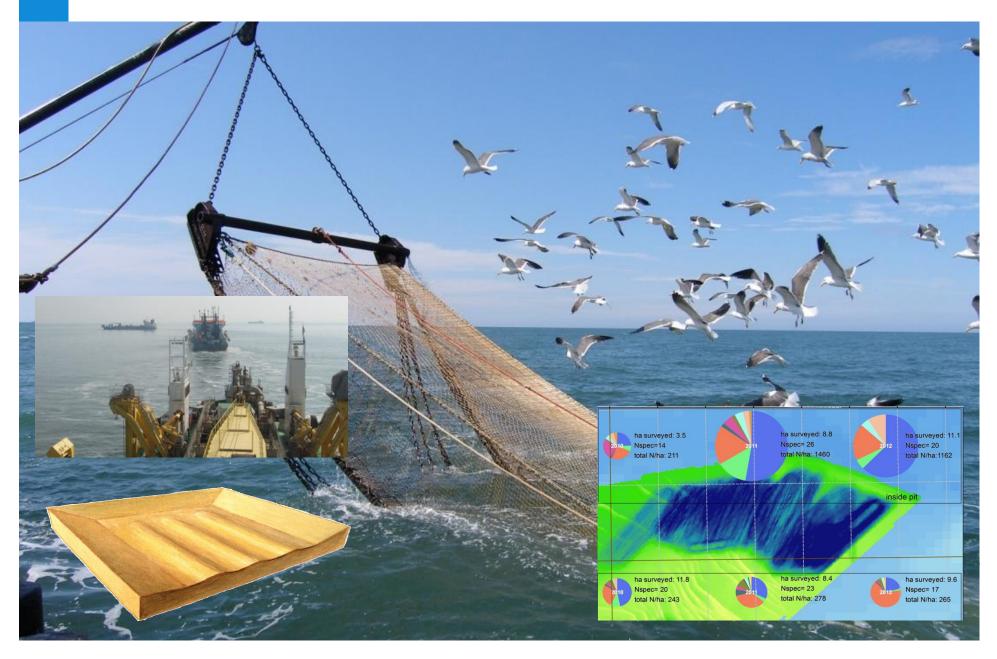








Knowledge for infrastructure projects



Construction

28 maart 2011

















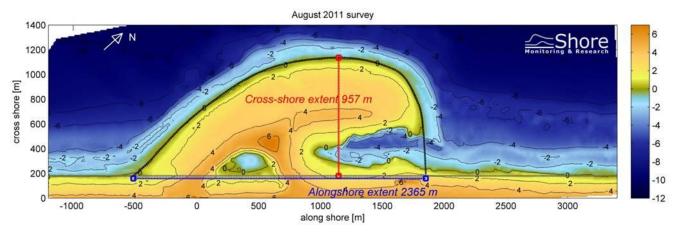


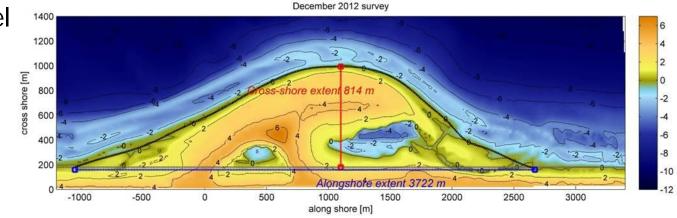
Recreation and Nature



Morphology: General observations

- Erosion seaward side ('tip')
- Sedimentation southern end
- Spit and channel formation near lagoon
- Symmetry



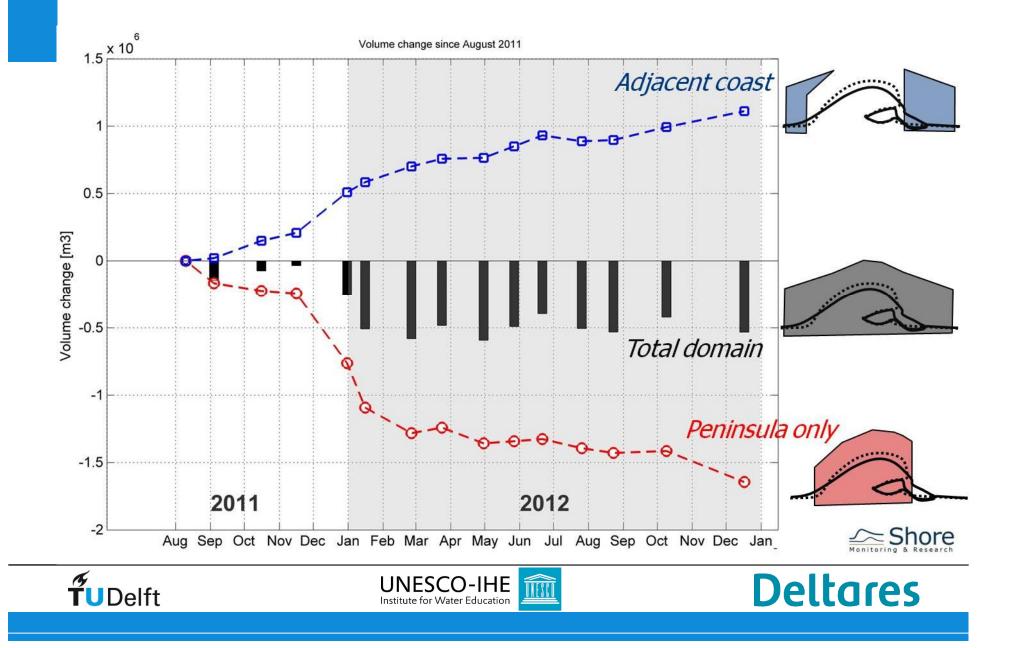


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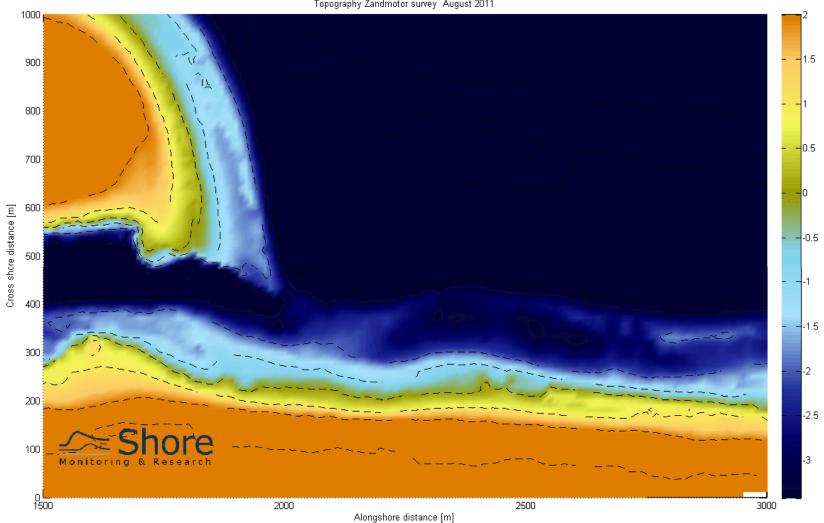




Sediment Budget

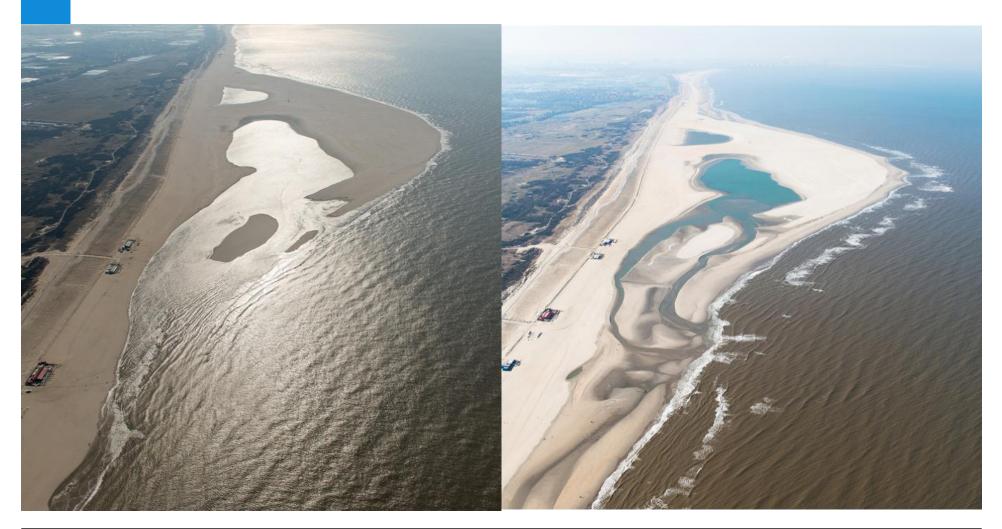


Spit and channel formation near lagoon



Topography Zandmotor survey August 2011







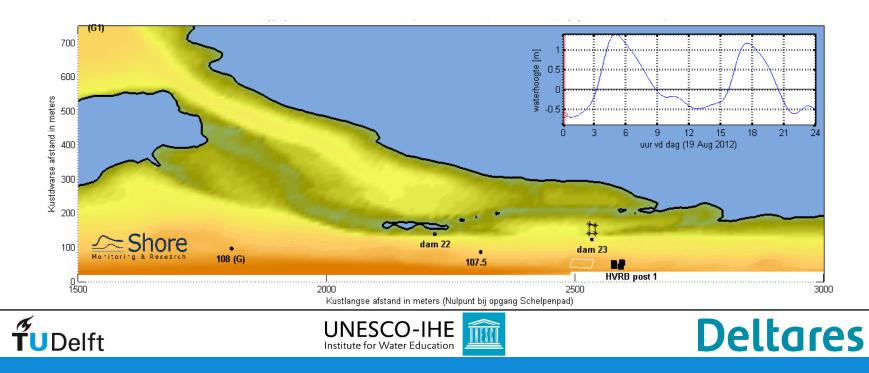


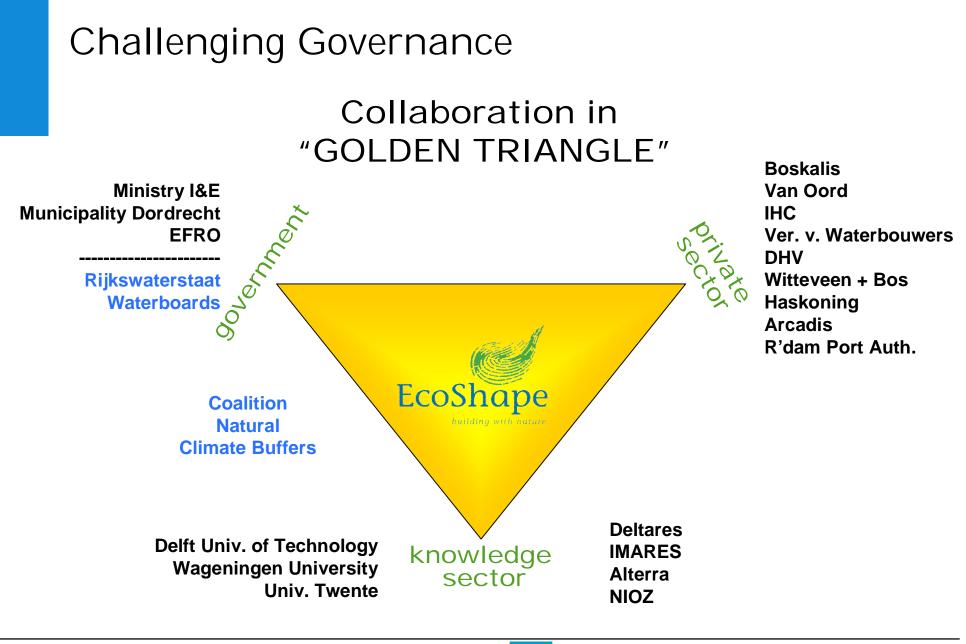


Vertical tide















Challenging Governance MEGASTORT VAN ZAND MOET KUST WESTLAND VERSTERKEN

Mens maakt zand Bij Ter Heijde, tussen emet nieuwo

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AD/Haagsche Courar 21 augustus 2013 woens 14 mei 2013 dinsdag

Regio - Den Haag; Biz. 1

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De reddingsbrigade ervaren surfers die ledereen wil het pro is als ze wat dichter

Daamaast heeft de Ouverling: We heb zoekacties.

20 August 2013

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Binnenland; Blz. 7

357 woorden

Brigades ba Gevaarborden bij ;

Rebecca van de Kar

- Schiereiland voor Zuid-Holland r

De gemeenten Den Haag en We Zandmotor, het kunstmatige sch incidenten met recreanten die zi

Bij de incidenten kwamen een g van de Zandmotor. Zij werden o konden, en gered moesten wor

De Zandmotor is een in 2011 a de kust bij Zuid-Holland moet stroming, wind en golven verp stuk strand, van zo'n twee kil afgezonderd raken van de ku

Uit vergelijkend onderzoek b recreanten zich laten verrass onderzoekers. Langs de hel waarschuwingsborden gepla: een veilige looproute over d.

Kitesulfen is de lat

gaat aan de sl

PVV stelt vragen over veiligheid zwemmers bij Zandmotor

Gepubliceerd op : vrijdag, 10 juni 2011 - 17:13

DEN HAAG - De PVV in Den Haag heeft het college van Burgemeester en Wethouders vragen gesteld over uitbreiding van het zwemverbod bij de Zandmotor voor de Scheveningse kust.

Aanleiding is het vermoeden van de PVV dat

zwemmen bij de Zandmotor gevaarlijker is dan eerder werd gedacht. De partij wil de garantie van het college dat zwemmers en recreanten veilig zijn als ze zwemmen in dat gebied.

De PVV nam de veiligheidssituatie rond de Zandmotor al eerder op de korrel. De partij publiceerde in november vorig jaar op zijn website over gegevens te beschikken, waaruit bleek dat het project ook de drinkwatervoorziening van zo'n

Tags: veiligheid, zandmotor

Voor een deel van het gebied, aan de buitenkant van zeestromingen tevens een zwemverbod. Eigenaren van strandpavigoen dagomzet. Zij stellen dat zvemverboden niet nodig zouden zijn als gemeentelijke weer reddingsbrigades gerichter zouden surveilleren. Voor het gebied langs de kuststrook gold tot vonge zwemverbod, maar dit is door afname van de stroming opgeheven.

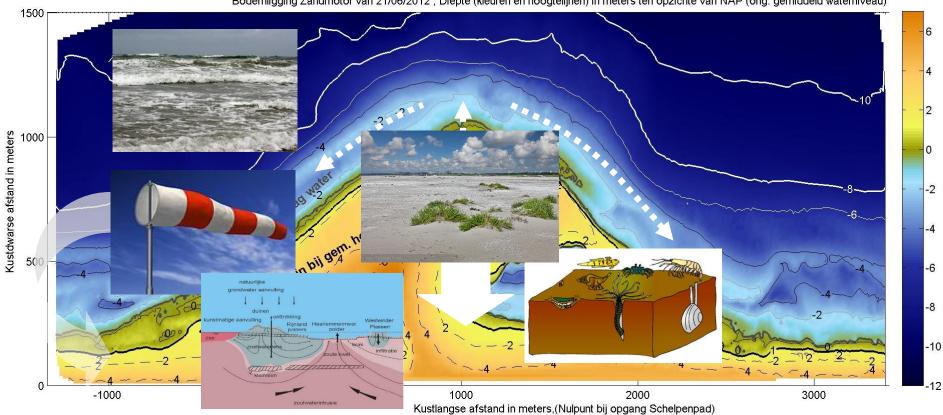


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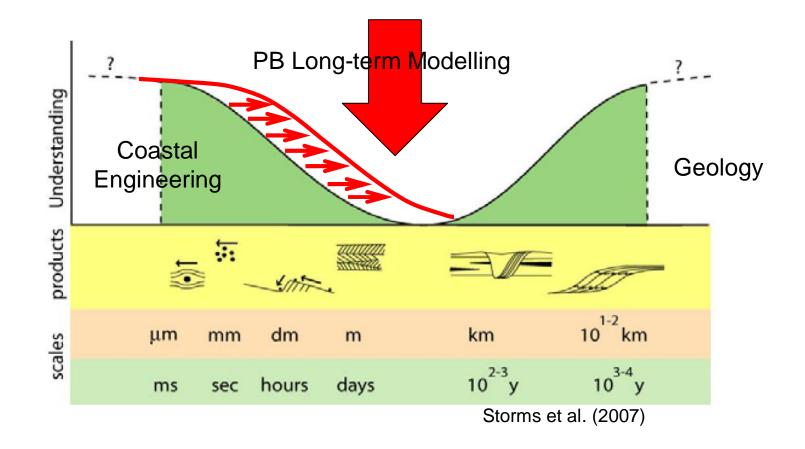
Understanding of landscape dynamics: inter-disciplinary knowledge



Bodemligging Zandmotor van 21/06/2012, Diepte (kleuren en hoogtelijnen) in meters ten opzichte van NAP (ong. gemiddeld waterniveau)



Different time scale:









Extensive monitoring campaign

BEACH





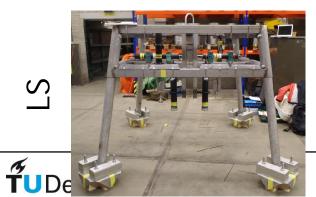


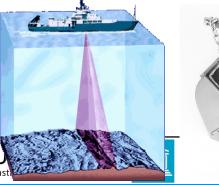
SURF





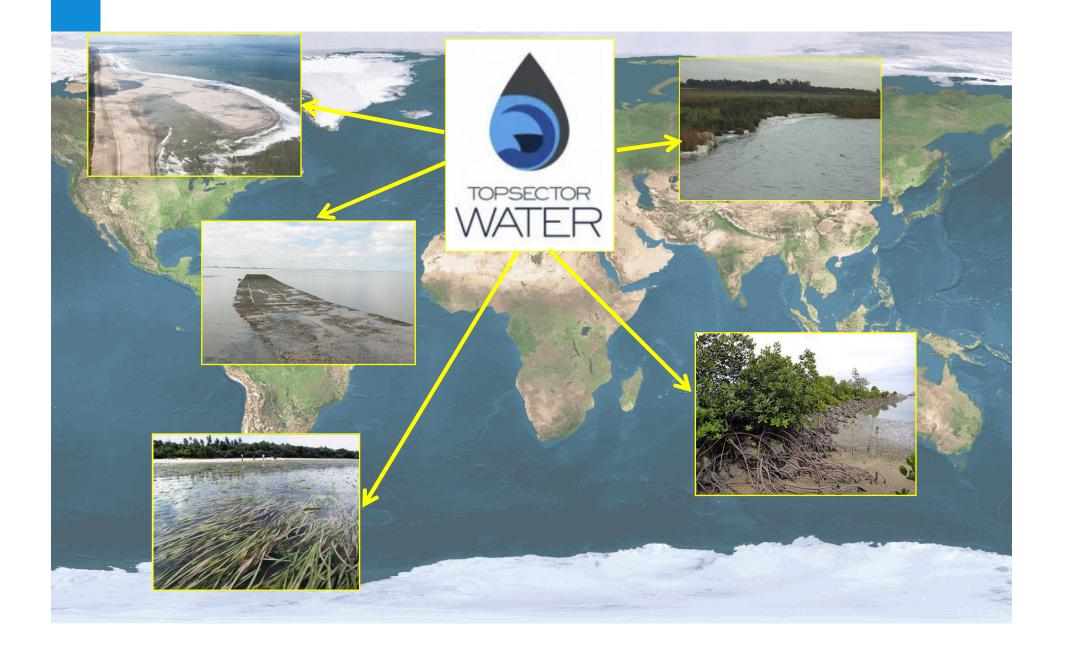








Explore new applications...



Modellling event driven erosion XBeach

Dano Roelvink, Ad Reniers, Ap van Dongeren, Jaap van Thiel de Vries, Robert McCall, Arnold van Rooijen







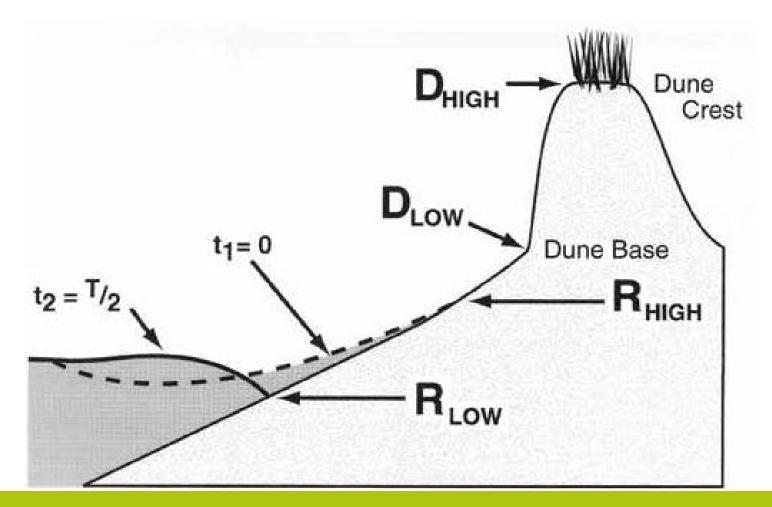
Challenge the future

Controlling factors in storm impact:

- Hydrodynamic boundary conditions
 - Surge properties (surge height, temporal and spatial surge level gradients)
 - Wave properties (Wave height, Wave period, Spectral shape)

- Coastal properties:
 - Crest height of dunes
 - Sediment properties
 - Vegetation
 - Longshore variation in topography and bathymetry
 - Presence of structures

Storm regimes (Sallenger, 2000)

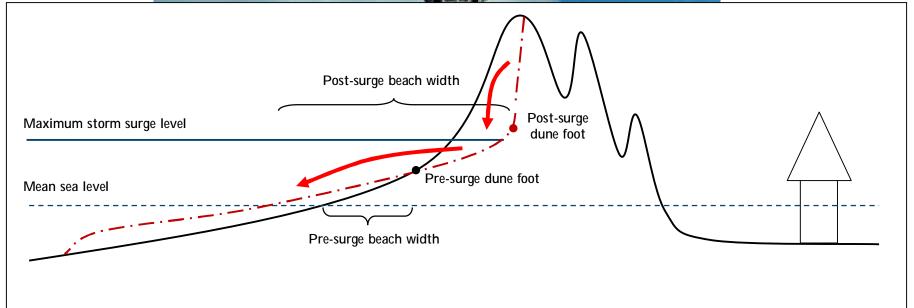


Inundation: Wave rundown above Dune Crest:

$$R_{LOW} > D_{HIGH}$$

Collision / Dune Erosion









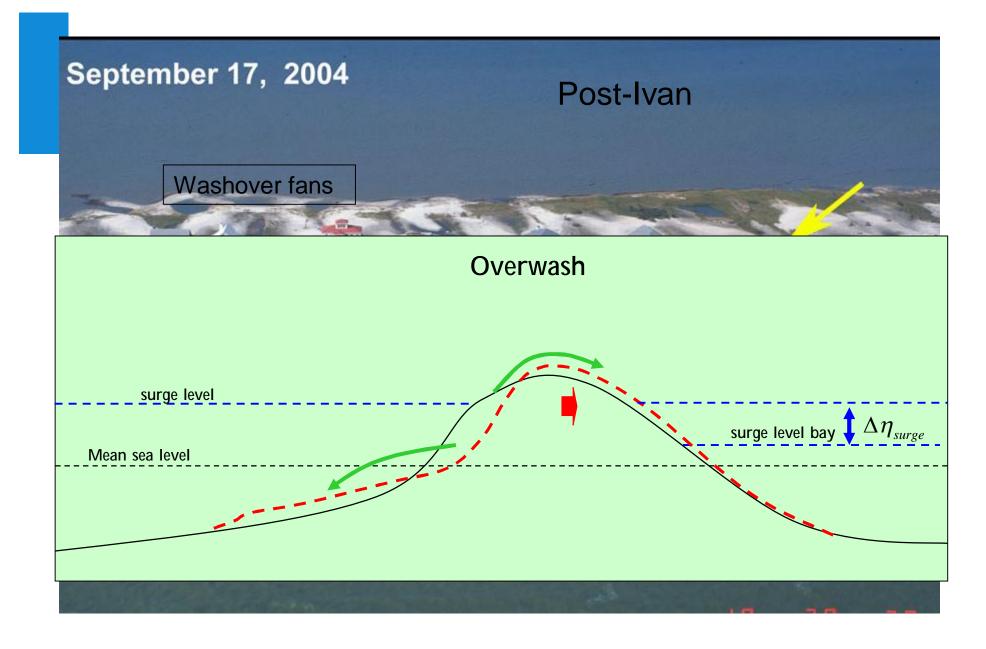








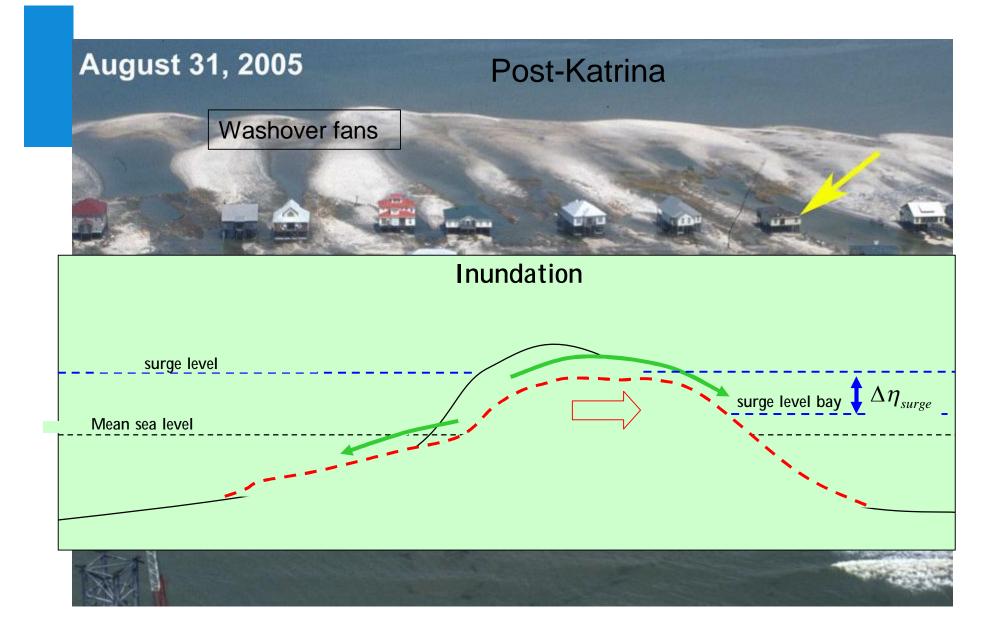








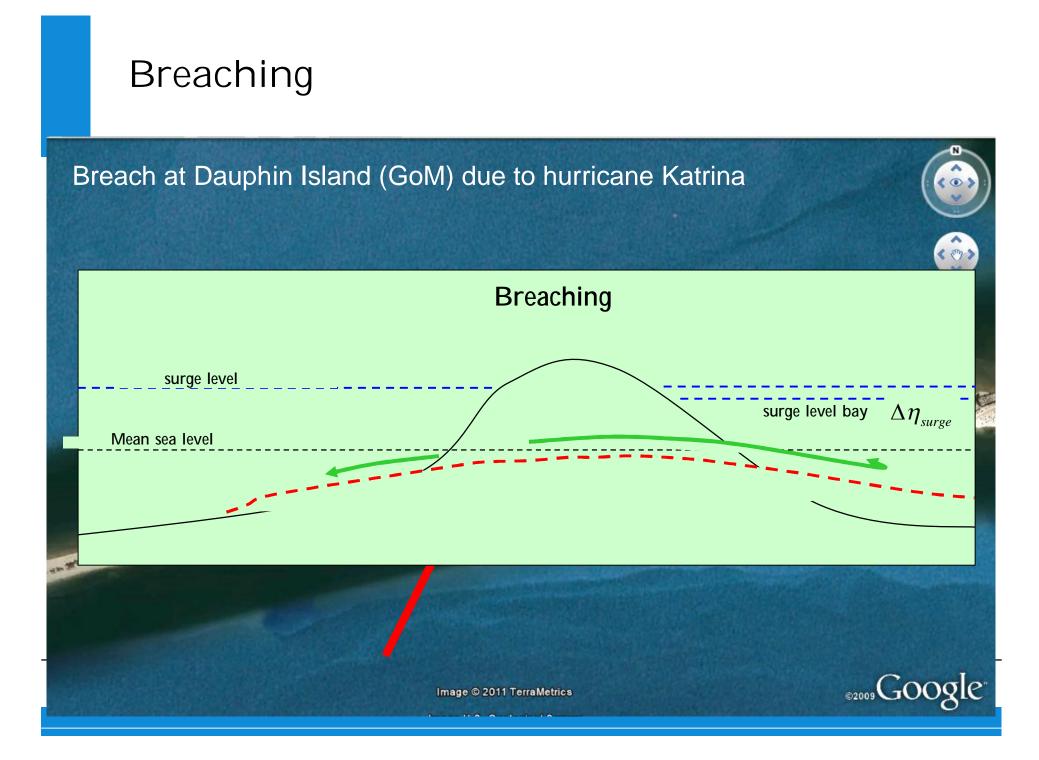




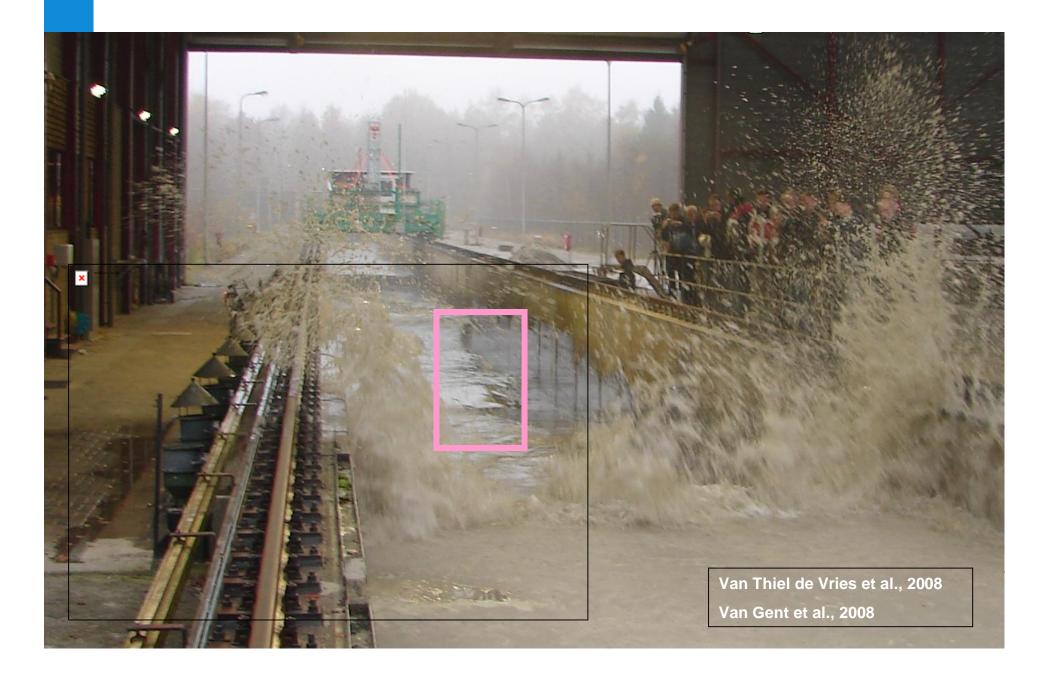








Near shore processes during storms

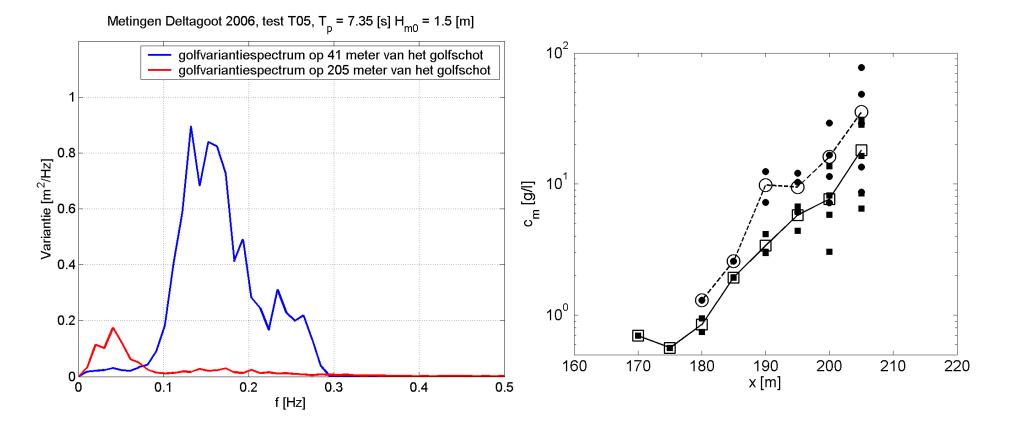


Near shore processes during storms

Wave spectra:

Near dune sediment suspensions:

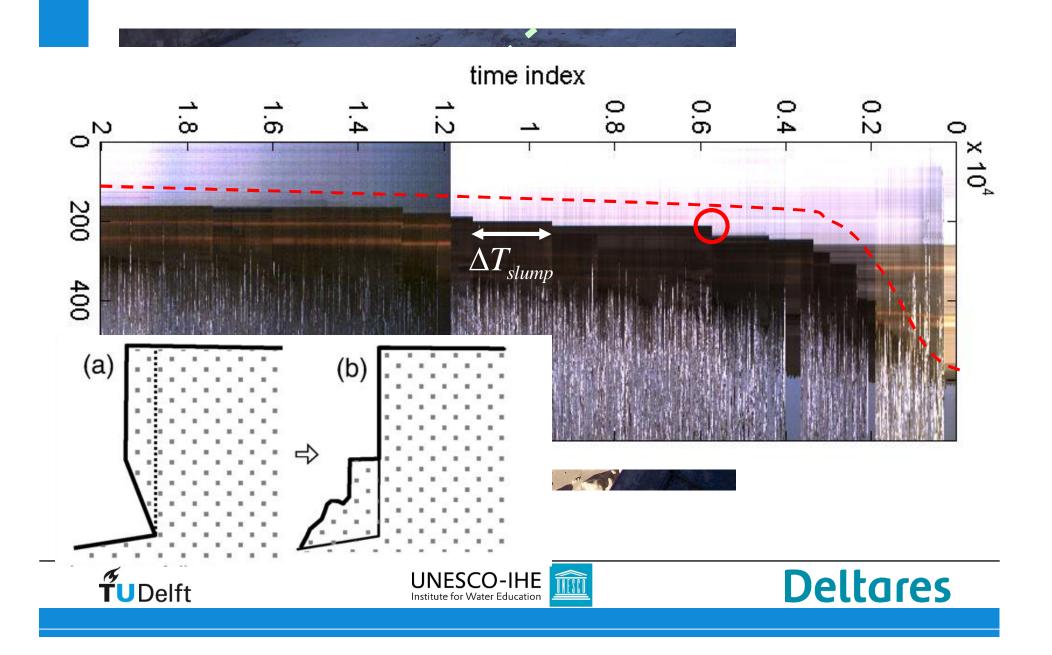
Deltares



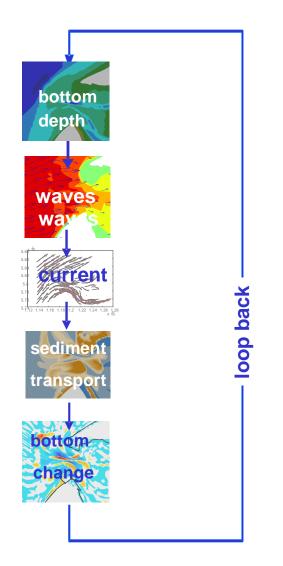




Dune face erosion



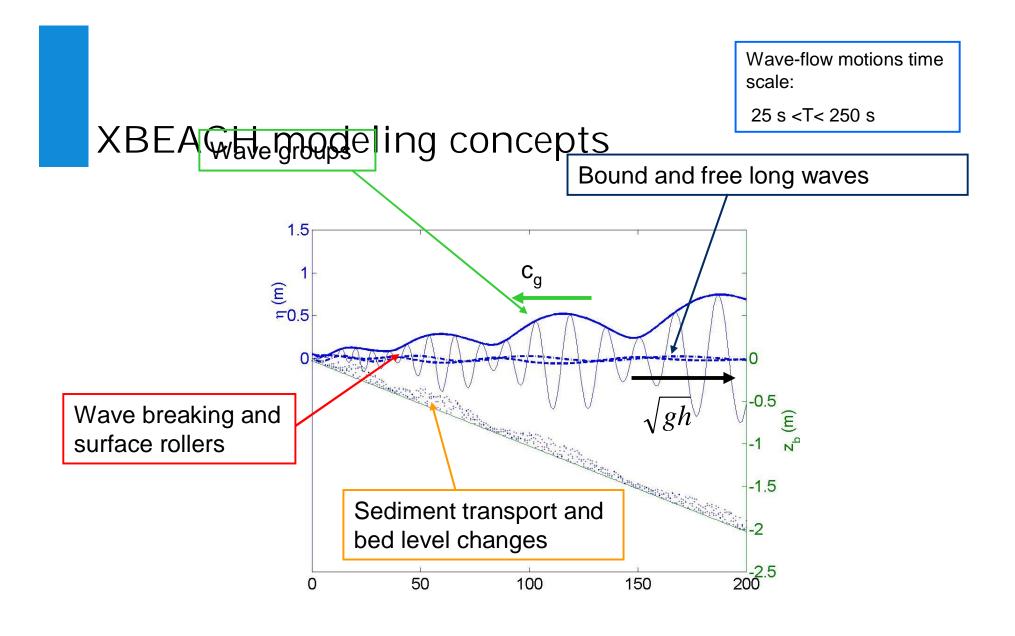
XBEACH Model set-up









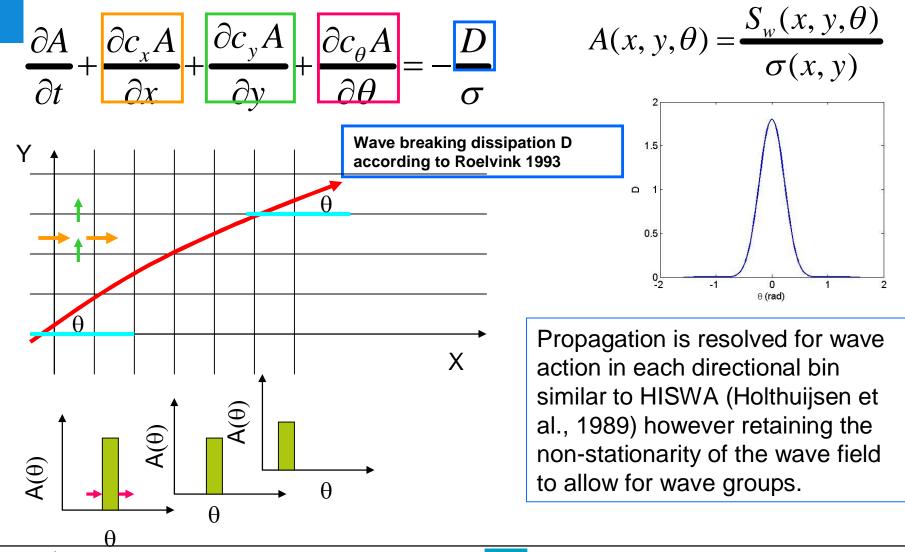








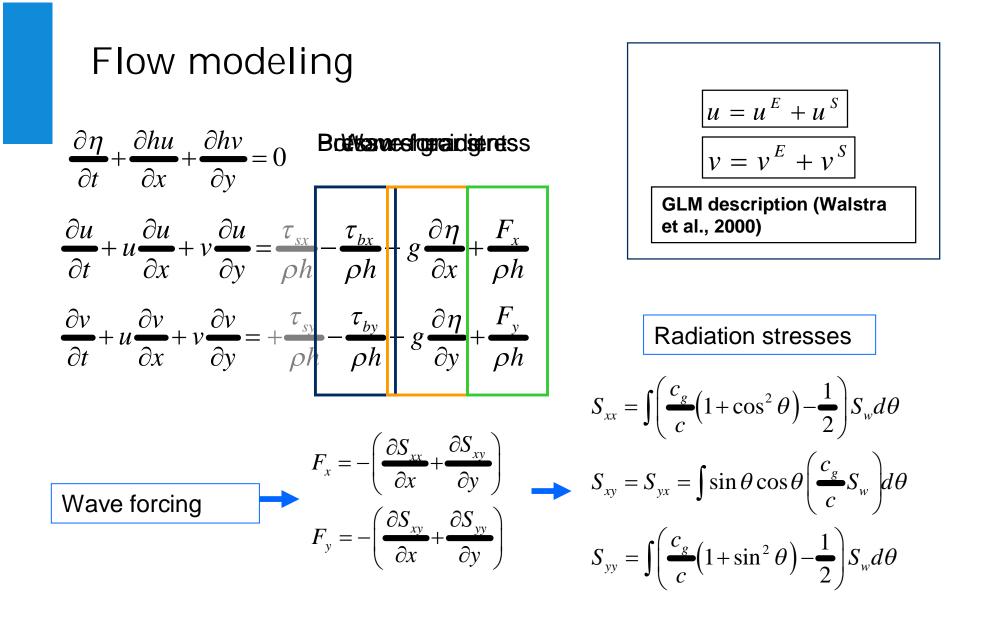
2D-wave action balance



Section 5.2 CD1, wind waves







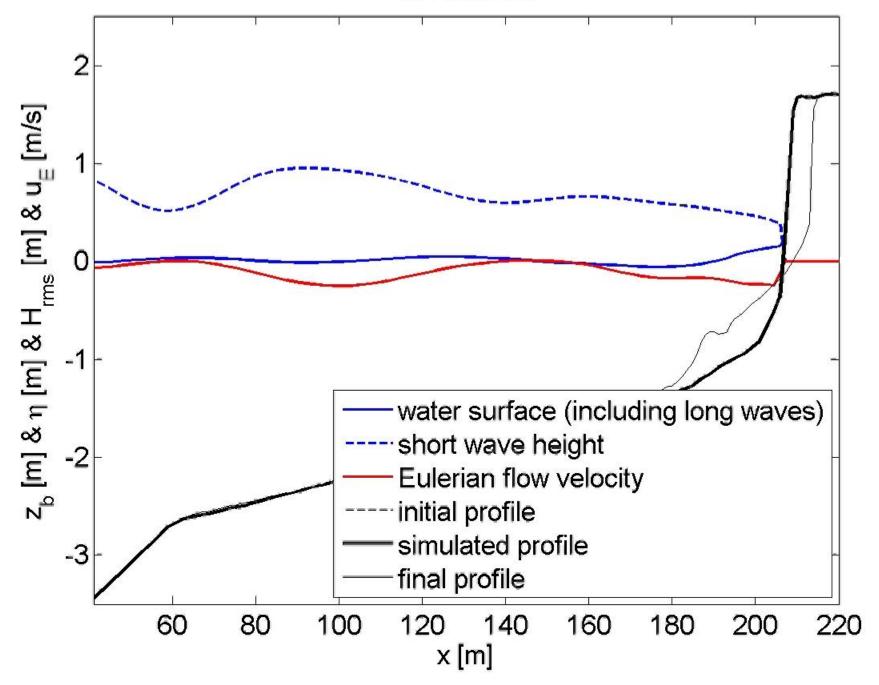




Deltares

Surf Beat: Boundary Conditions $E_{w}(x,t) = \frac{1}{2}\rho g |A_{low}(x,t)|^{2}$ Hilbert Transform Տղղ [m²/Hz] f_{m-1,0} f split А, п [m] f [Hz] $\eta(x,t) = \sum_{i=1}^{N} \hat{\eta}_{i} e^{i(\sigma_{j}t - k_{x,j}x + \phi_{j})} + *$ $j = \overline{N_{split}} + 1$ $\eta(x,t) = \sum_{i=1}^{N_{split}} \hat{\eta}_j e^{i(\sigma_j t - k_{x,j} x + \phi_j)} + *\overline{-\mathrm{IHE}}$ T [s] Deltares

0.2 minutes



Sediment transport

$$\frac{\partial hC}{\partial t} + \frac{\partial hCu^{E}}{\partial x} + \frac{\partial hCv^{T}}{\partial y} + \frac{\partial}{\partial x} \left[D_{h}h\frac{\partial C}{\partial x} \right] + \frac{\partial}{\partial y} \left[D_{h}h\frac{\partial C}{\partial y} \right] + \frac{hC_{eq} - hC}{T_{s}}$$
Eq. 6.52 CD1
$$C_{eq} = \frac{A_{sb} + A_{ss}}{h} \left(\left(|u^{E}|^{2} + 0.018\frac{u_{rms}^{2}}{C_{d}} \right)^{0.5} - u_{cr} \right)^{2.4} (1 - \alpha_{b}m) \quad \text{Soulsby-van Rijn, 1996}$$
avalanching
Bottom update:
$$1 - p)\frac{\partial z_{b}}{\partial t} + \frac{\partial S_{x}}{\partial x} + \frac{\partial S_{y}}{\partial y} = 0$$
Eq. 6.14 CD1
$$\Delta z_{b} = max \left(-\Delta t \left(\frac{\partial z_{b}}{\partial x} - m_{cr} \right) \Delta x, -0.005 \right) , \frac{\partial z_{b}}{\partial x} < 0$$

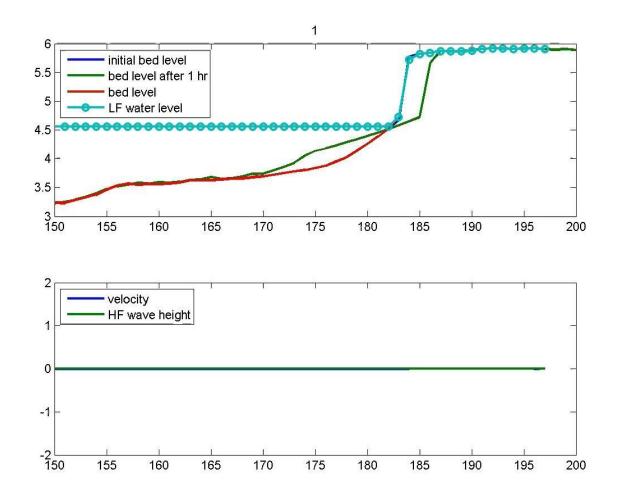


(1





Avalanching

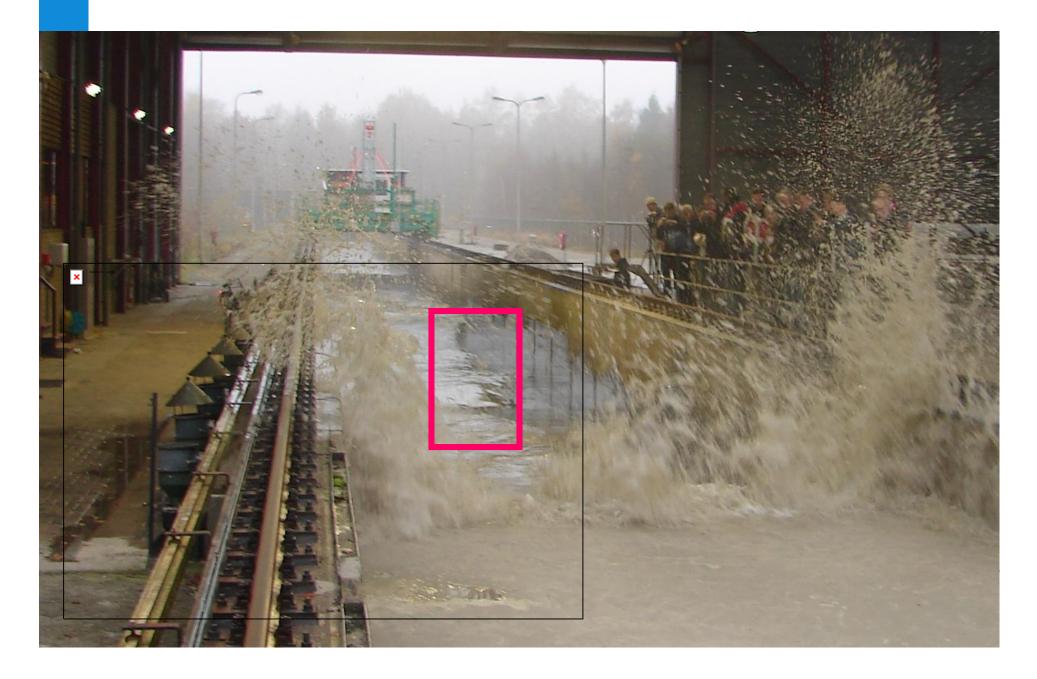




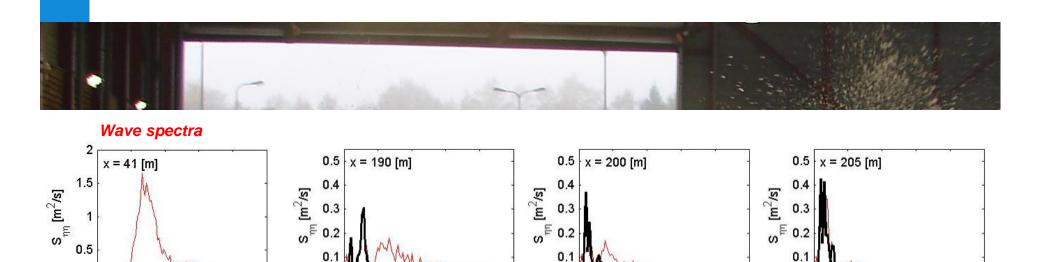


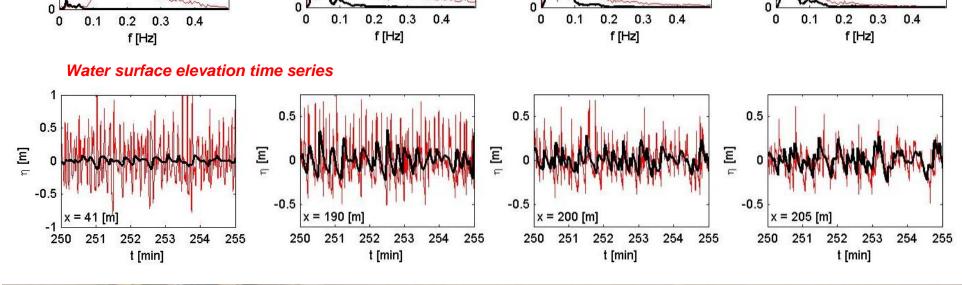


Large scale dune erosion tests



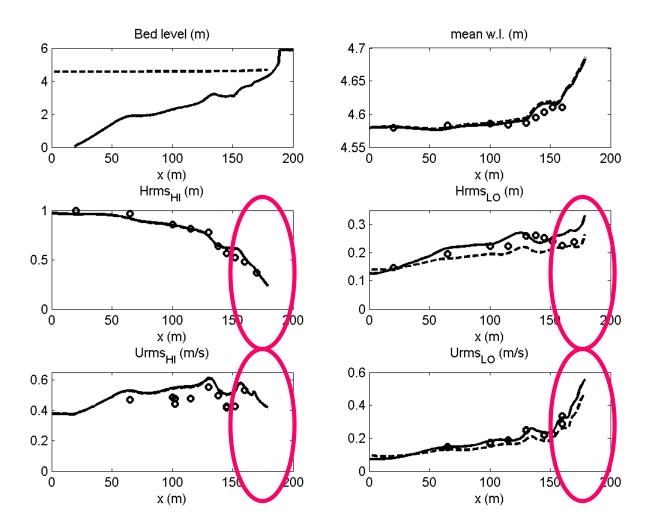
Dune erosion case: Deltaflume test







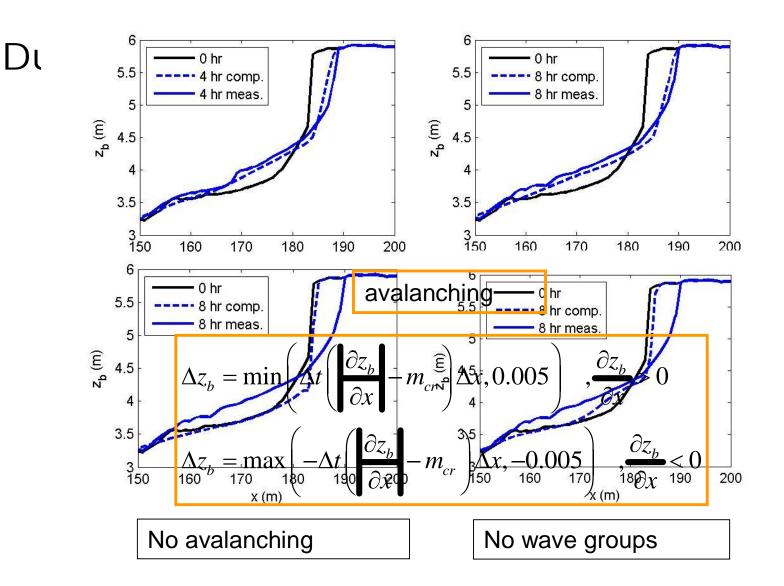










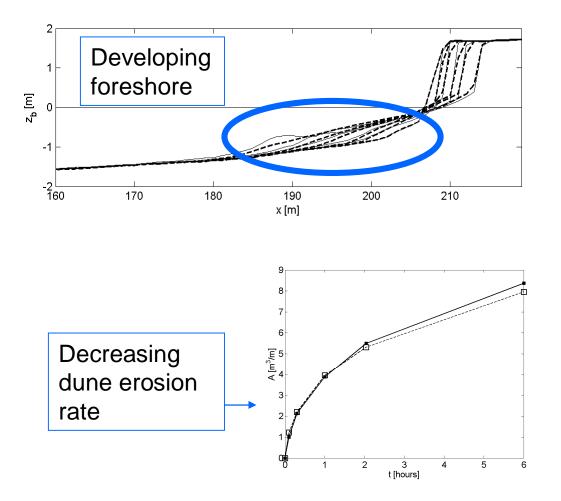








Temporal evolution



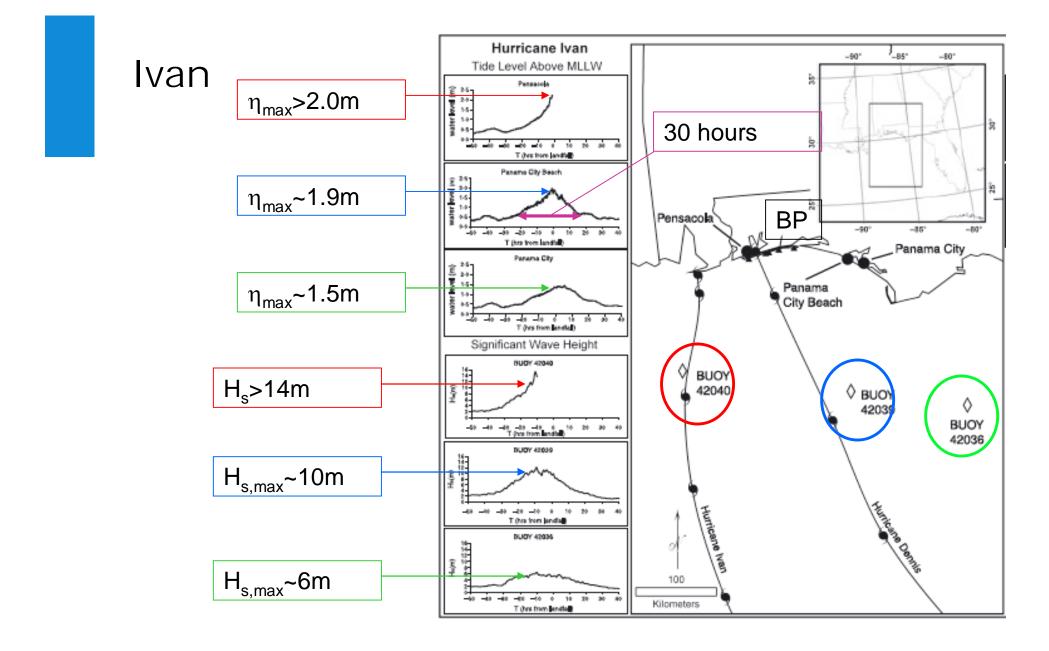








© 2007 Europa Technologies Image © 2007 DigitalGlobe







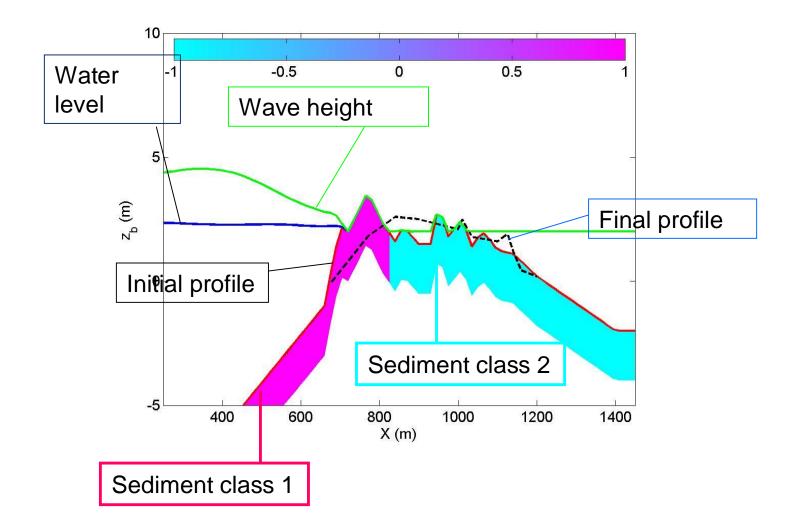


1D Model setup

Significant wave height H 10 m Peak frequency 0.09 Hz Surge level 1.9 m Duration 15 hours

© 2007 Europa Technologies Image © 2007 DigitalGlobe ^{©2007}Google™

Overwash modeling

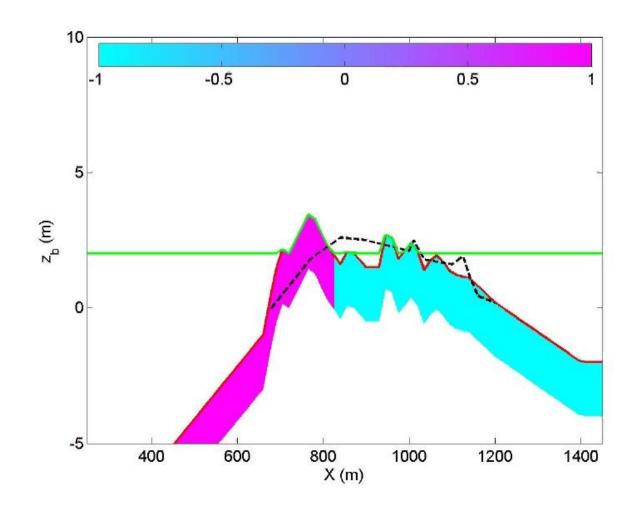


ÎNESCO

Initiation Dal point from Wang and Horwitz, 2000 Institute for Water Education



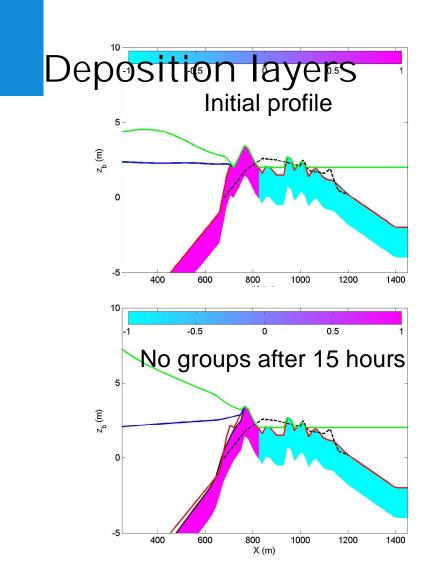
Simulation

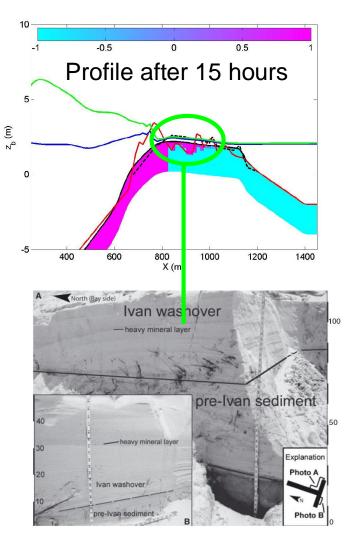












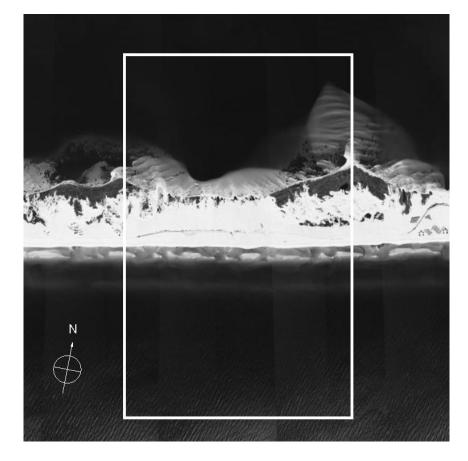
Courtesy of Wang and Horwitz, 2006

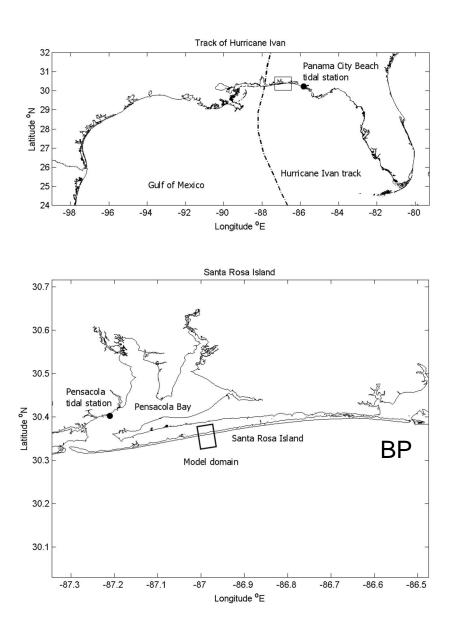






Alongshore variation



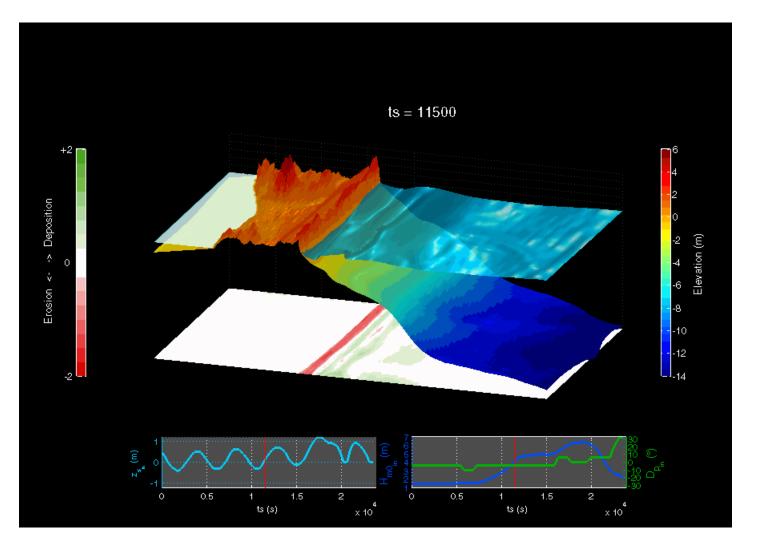








Collision \rightarrow Overwash

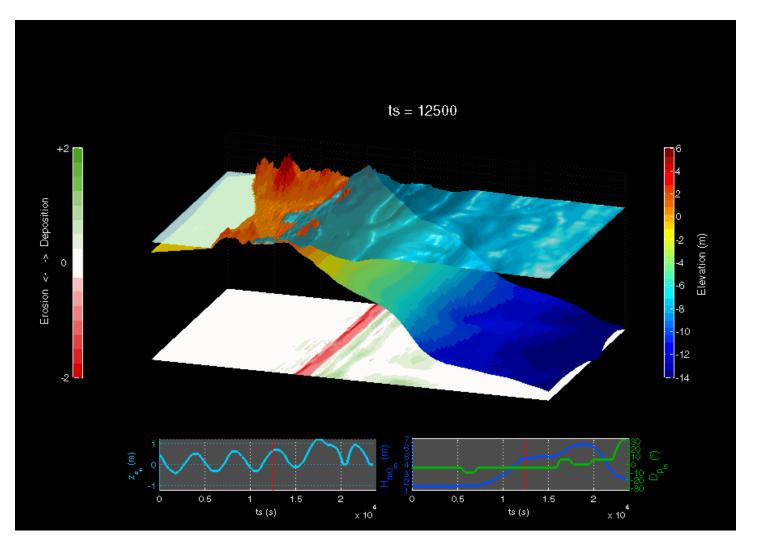


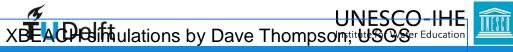


 UNESCO-IHE

 XBEADE iffulations by Dave Thompsom;

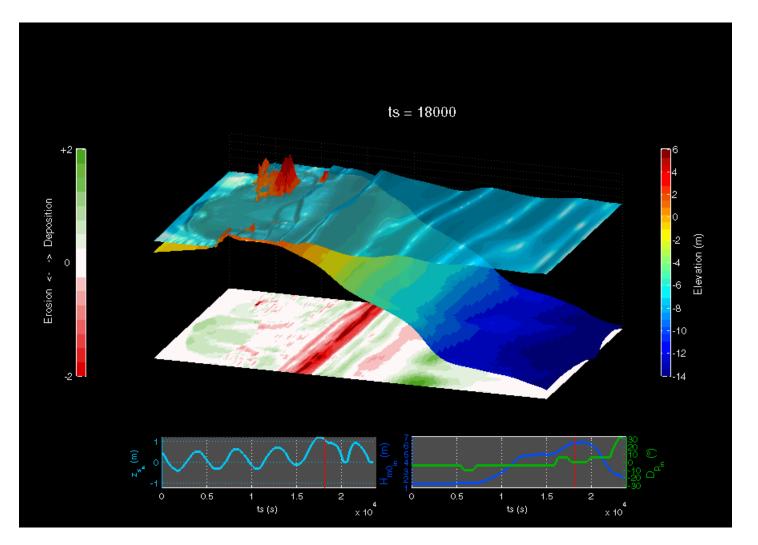
Overwash







Peak of the Storm: Inundation





 UNESCO-IHE

 XBEADE iffulations by Dave Thompsom;

Breaching Case: Zwin

• MS4

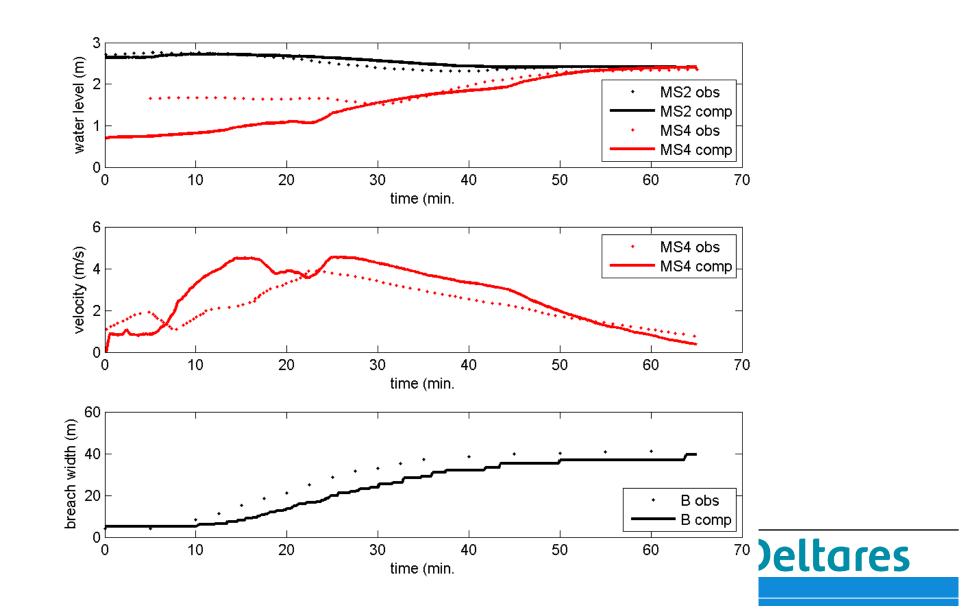
B: Breach (width)

MS2

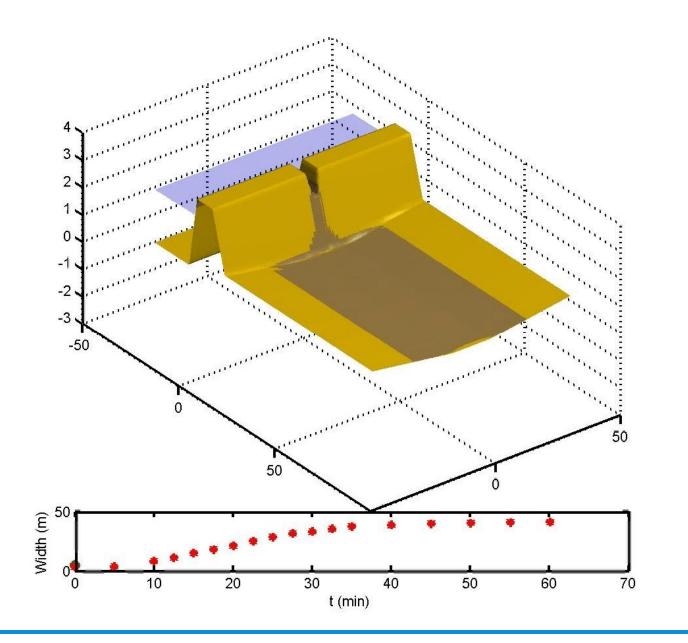
MS2: Water

MS4: Water level and flow velocity

Breaching Case: Zwin



Breaching Case: Zwin



ŤUC

Part II

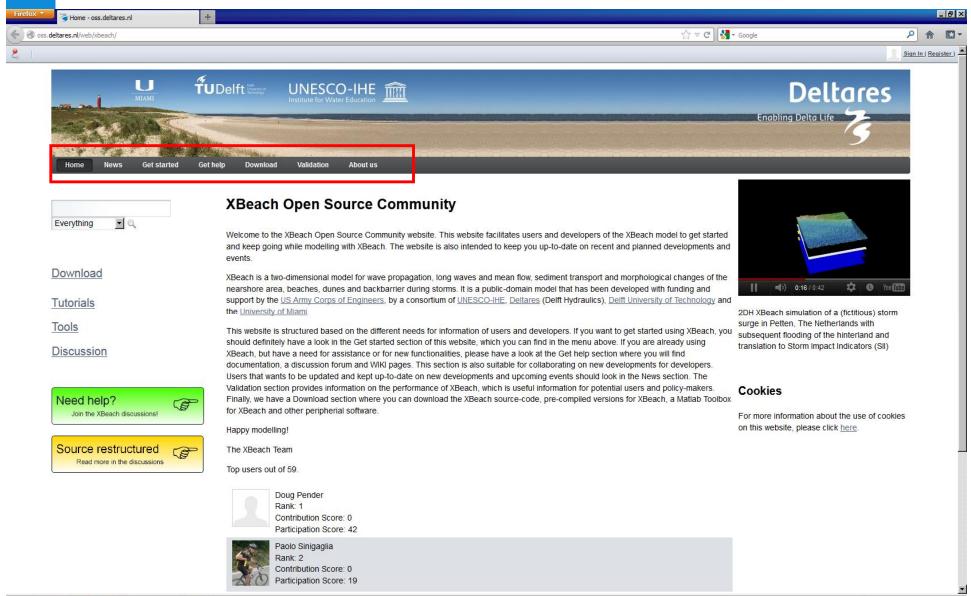
Hands on: Modelling Event Driven Erosion







XBeach.org (accessible via oss.deltares.nl)



Running XBeach:

- 1. Simulation folder where you collect the following files:
- 2. XBeach executable
- 3. Params.txt file
- 4. Depth file

Additional Files:

- Grid file(s): In case you work with non-equidistant grids
- Wave input files: This can be a list of (irregular) wave conditions
- Waterlevel input files: In case you want to apply varying tide and surge conditions
- Files related to additional functionality: i.e. to specify structure, ground water flow, tracers, river discharge.







Running XBEACH: Tips and Tricks

- Setting up a Grid:
 - Grid resolution should be sufficient to describe long wave
 - Vary grid resolution based on Courant condition
 - Near water line, grid resolution based on expected morphological changes
- Define Depths:
 - Offshore boundary at sufficiently deep water for realistic long wave boundary conditions (n < 0.8)
 - Uniform coast (three cells) near lateral boundaries and offshore boundary
- Settings:
 - Use defaults as much as possible (especially when you start)
- REMARK: Tricks for robuust model set-up are implemented in Toolbox







Getting Started (1)

- 1. All will receive hardcopy assignments and a USB stick that contains model software, documentation and software.
- 2. Copy all data to a local folder on your laptop and wait for further instructions.
- 3. Go to folder Documents → Exercises and follow the instructions in Install_Delft3Dsoftware.doc
- 4. Work on the following examples:







Part II

Advanced applications







Contents

- Situations with hard elements
 - Dune revetments
 - Coral reefs
- Situations with vegetation (mangroves)
 - Mangroves
- Non-hydrostatic model and ground water flow
 - Gravel beaches
- Long term simulations







r1

Slide 120

r1	dit kan weg?
	rooijen; 26-11-2012

Part II

Situations with hard elements:

- Dune revetments
- Coral reefs







Hard layers

• Hard structures substantially affect the morphodynamic evolution during a storm in both cross-shore and longshore direction









Hard Elements

- •Implementation:
- You specify the sediment thickness on top of a hard layer.
- In case the sediment thickness on top of the layer becomes sufficiently small the sediment source term is limited:

$$\frac{\partial hC}{\partial t} + \frac{\partial hCu^{E}}{\partial x} + \frac{\partial hCv^{E}}{\partial y} + \frac{\partial}{\partial x} \left[D_{h}h\frac{\partial C}{\partial x} \right] + \frac{\partial}{\partial y} \left[D_{h}h\frac{\partial C}{\partial y} \right] = \min\left(\frac{hC_{eq} - hC}{T_{s}} \right)$$

In which

$$S_{\max} = (1 - p) \frac{dz_{remain}}{dt}$$







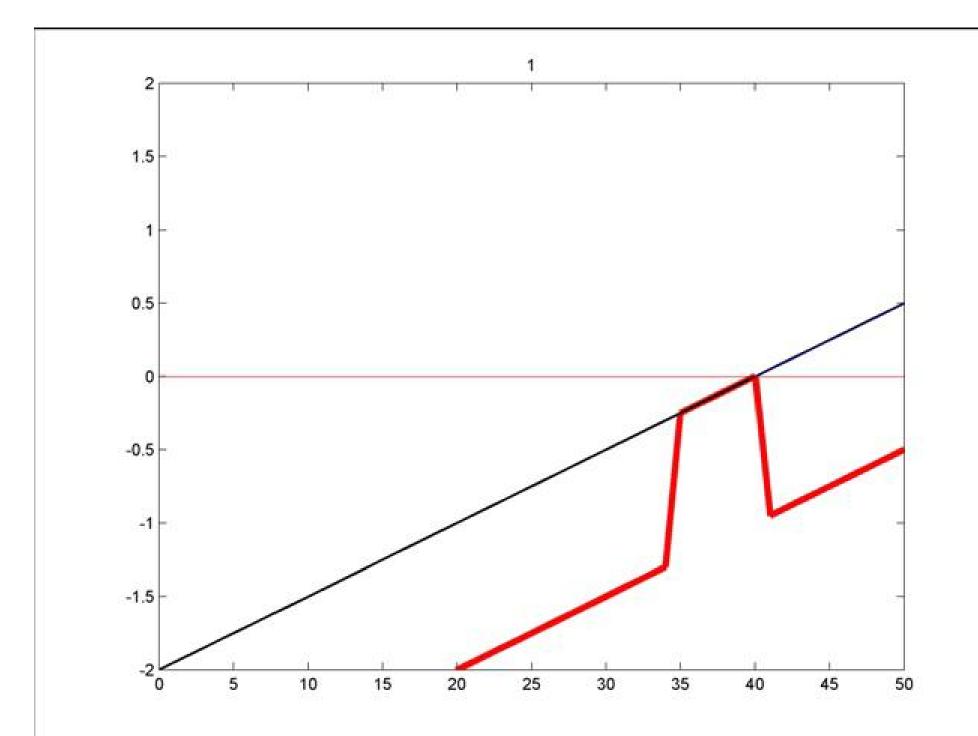
Hard Layers

- To setup a model with a hard layer two additional keywords need to be specified in params.txt:
 - struct: struct = 1 in case of a hardlayer and struct = 0 (default) in the abscence of hardlayer.
 - ne_layer: ne_layer is a filename that contains the thickness of the sediment layer on top of the hardlayer.

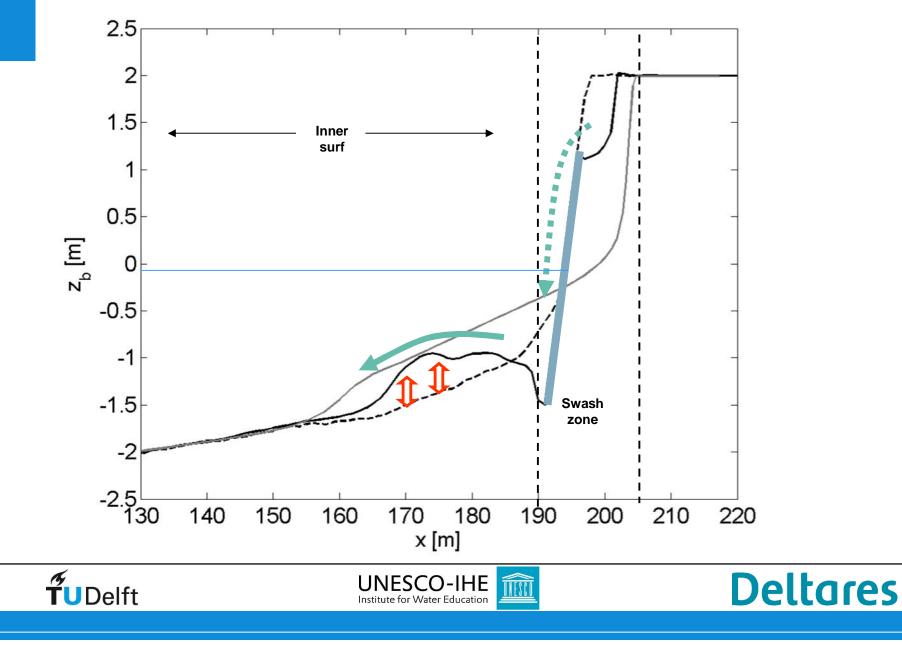








Dune erosion with revetment



XBeach: Including short wave run-up

- Include short wave run-up to simulate erosion above revetments:
 - Compute short wave run-up elevation at base of revetment from short wave height time series.
 - Simulate distribution of short wave run-up (without swash swash interactions):
 - concept of equivalence (Saville 1962: Batties 1974)

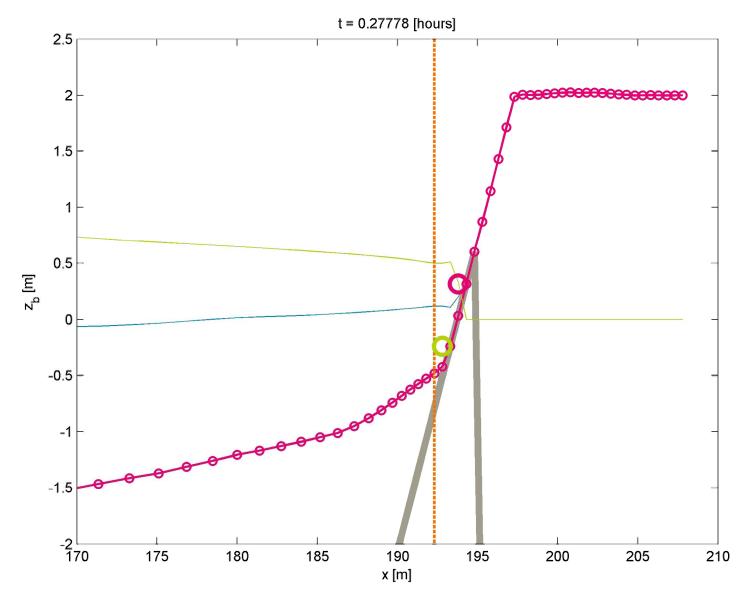
$$R = \gamma_{runup} H_{rms} \min(\xi, 2.3) \cos(\omega t)$$

$$\eta_{tot} = \eta_{wl} + R$$

$$\frac{\varphi_{tot}}{\varphi_{uot}} = \eta_{wl} + R$$

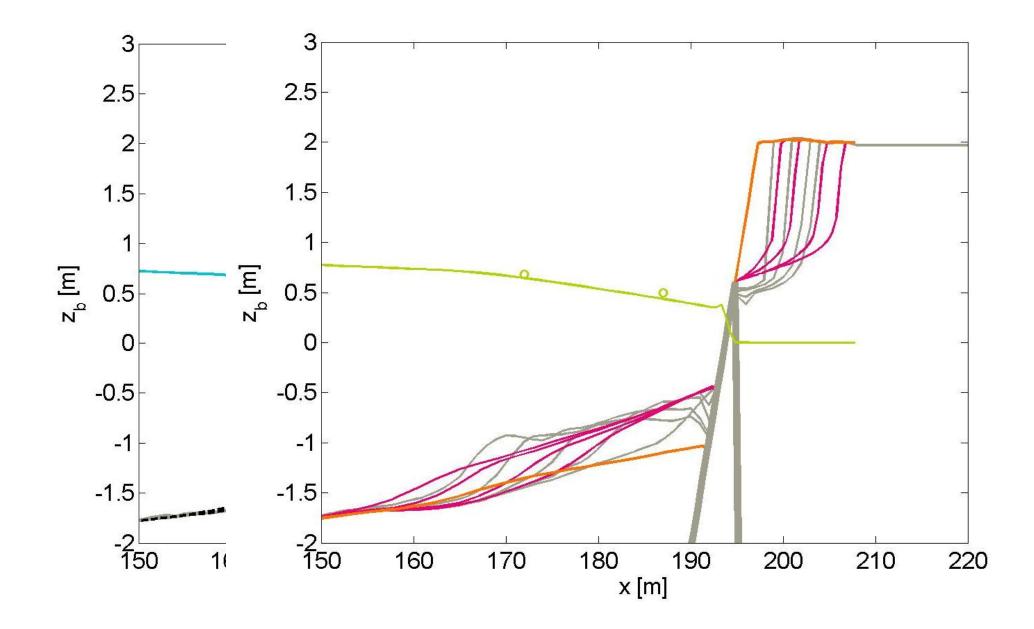
UNESCO-H
Institute for Water Education

XBeach: Including short wave run-up

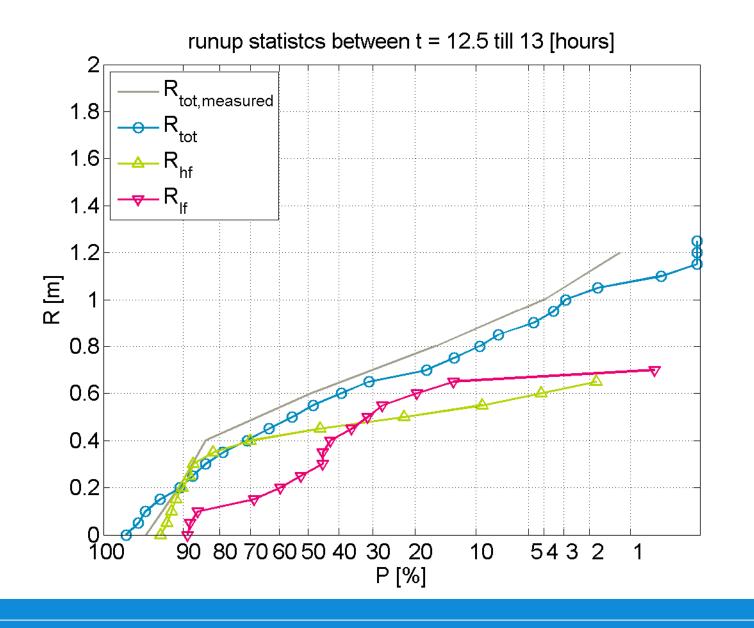


es

Results: Profile evolution



Runup statistics





Hard Layers

- To setup a model with a hard layer two additional keywords need to be specified in params.txt:
 - struct: struct = 1 in case of a hardlayer and struct = 0 (default) in the abscence of hardlayer.
 - ne_layer: ne_layer is a filename that contains the thickness of the sediment layer on top of the hardlayer.
 - swrunup: swrunup = 1 to account for short wave runup (default swrunup = 0)
 - facrun: facrun = 0.8 runup calibration factor (default facrun = 1)
 - jetfac: jetfac = 0.1 scout parameter (default facrun = 0)







Wave modelling in coral reef environments

- Coral reef systems are
 - present along large parts of tropical coastlines
 - protect the coast from storm impacts
 - form habitat for great number of species
- Waves and wave-induced currents are important to reef systems, drive
 - Sediment transports
 - nutrient dynamics,
 - Uptake by benthic communities
 - Wave run-up and overtopping of the main land or atoll.



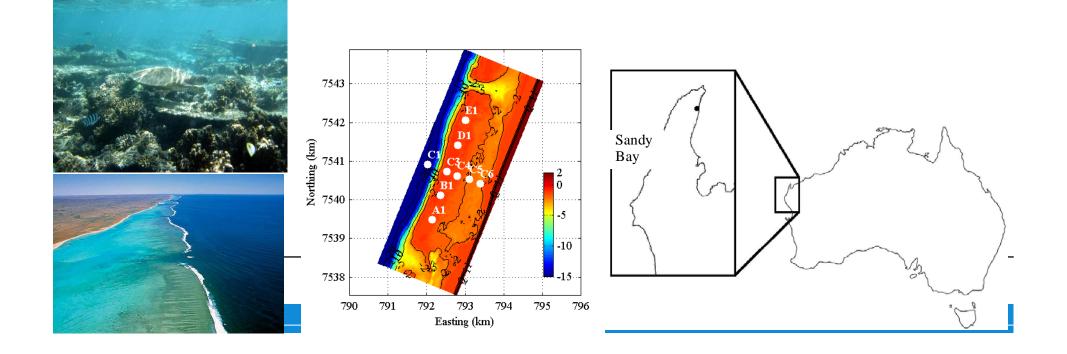




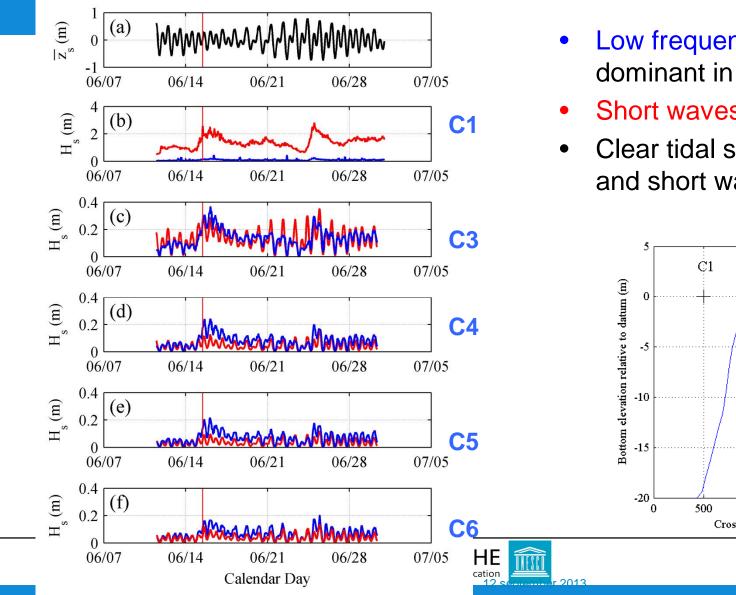
Ningaloo Reef Observations

Ningaloo Reef extends 250 km along the North-West Cape of Australia

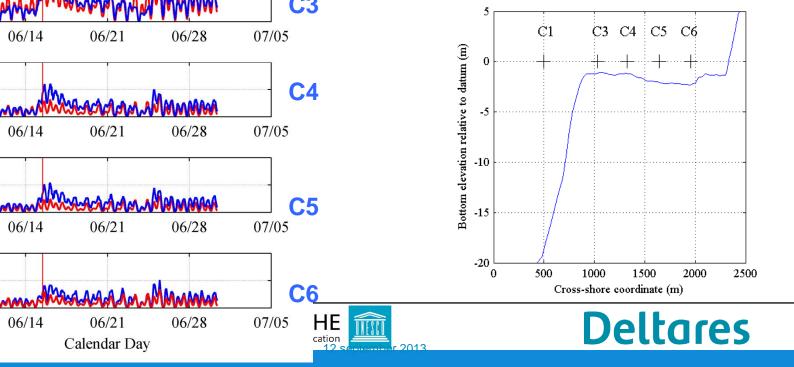
- Hundred individual reef-lagoon-channel circulation systems with gaps (channels) occurring in the reef every few kilometers.
- Swells from the South-West (roaring 40's).
- Field data by Ryan Lowe (U. of Western Australia) in 2009



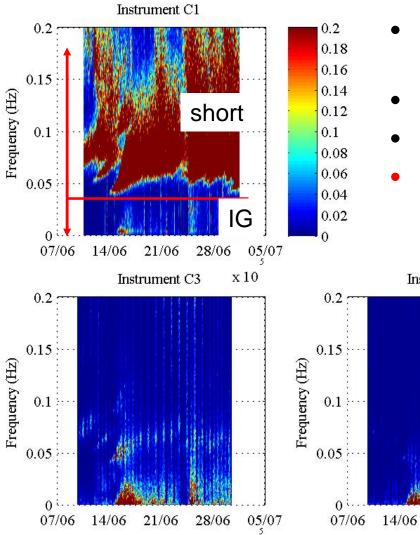
Short wave and IG wave heights



- Low frequency IG signal dominant in the lagoon
- Short waves decay
- Clear tidal signature of IG and short waves



Observations of spectra



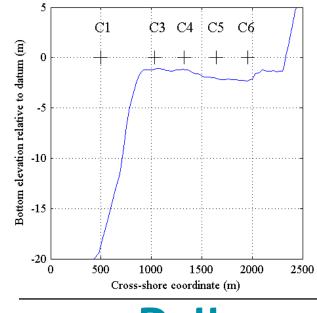
- Strong dissipation of short waves between C1 and C3
- Transfer to IG wave frequencies
- Can't model this with SWAN!
- So XBeach it is

28/06

05/07

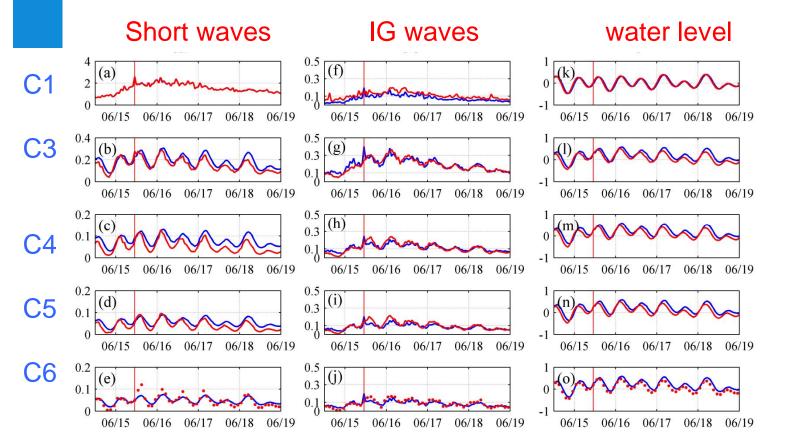
21/06

Instrument C4



<u>Deltares</u>

Results for storm duration 1D



Data

model

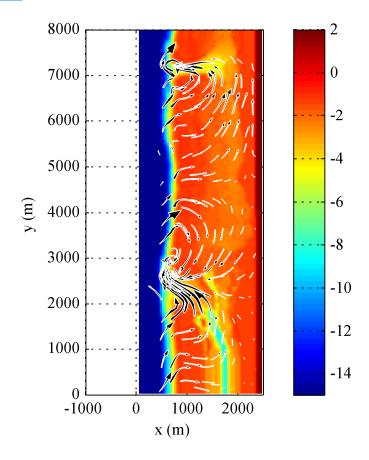
- Short waves slightly overpredicted
- Water levels slightly overpredicted
- Short waves and Infragravity wave displays tidal signature

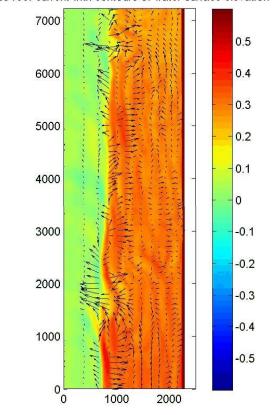




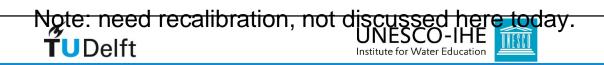


Now to 2D





Cross-reef current with contours of water surface elevation





Modification of equations

Wave action equation including bottom friction dissipation

$$D_f = \frac{2}{3} \rho \pi f_w \left(\frac{\pi H}{T_{rep} \sinh kh} \right)^3$$

- With free parameter f_w
- We use default settings, except calibration of short wave friction \mathbf{f}_{w} and
- unsteady current (IG) friction c_f.







Part II

Vegetation: - Mangroves







Vegetation: Mangroves

Mangroves are usually mildly sloped and the therefore dissipative

 Due to the dissipative character we hypothesize that wave group generated long waves play an important factor in mangrove morphodynamics and erosion

 We hypothesize that this effect is enhanced due to the presence of mangrove vegetation.









- Approach of Mendez and Losada (2004)
- Short wave attenuation by vegetation (wave action balance):

$$D_{veg} = -\frac{1}{2\sqrt{\pi}}\rho C_D b_v N_v \left(\frac{k}{2\sigma}\right)^3 \left(\frac{\sinh^3 k\alpha h + 3\sinh k\alpha h}{3k\cosh^3 kh}\right) H_{rms}^3$$

• Long wave attenuation by vegetation (momentum equation):

$$F_{veg} = 0.5C_D b_v N_v \frac{\alpha h}{h} u u$$

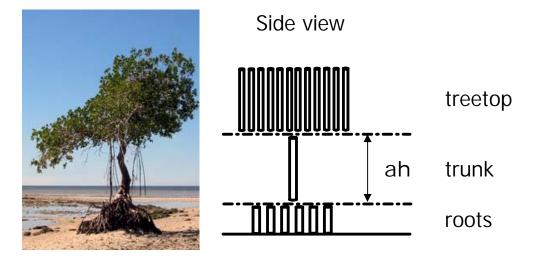




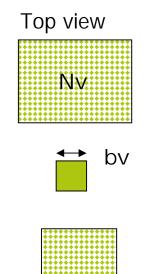


Vegetation in XBeach

Vertical structure of vegetation is accounted for



- Different species can be specified:
 - With different properties:
 - Section heights (ah)
 - Drag coefficient (Cd)
 - Number of plants per unit area (Nv)
 - Plant area per unit height (bv)

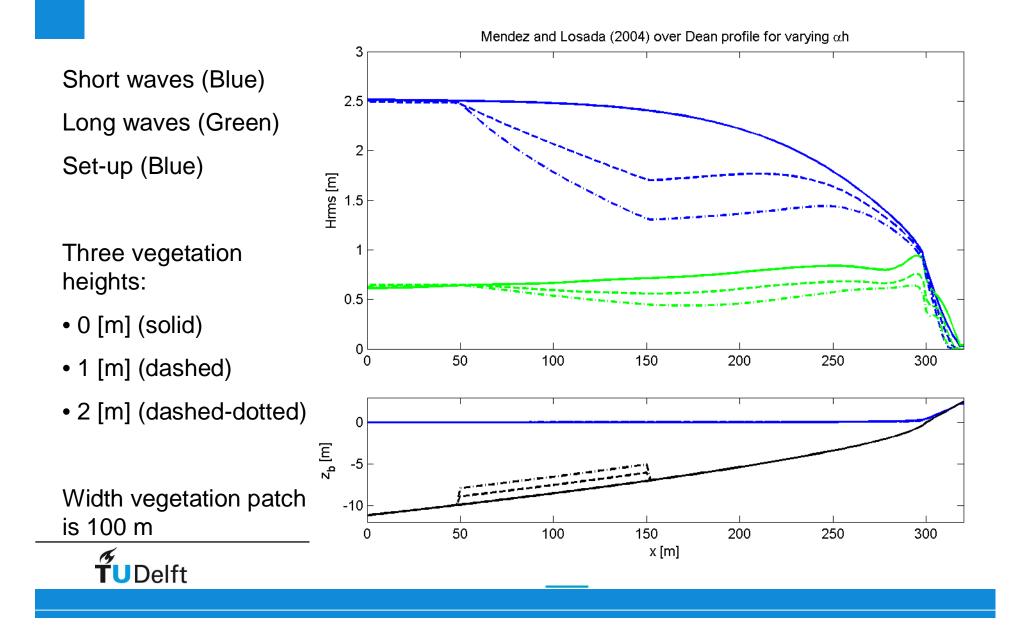




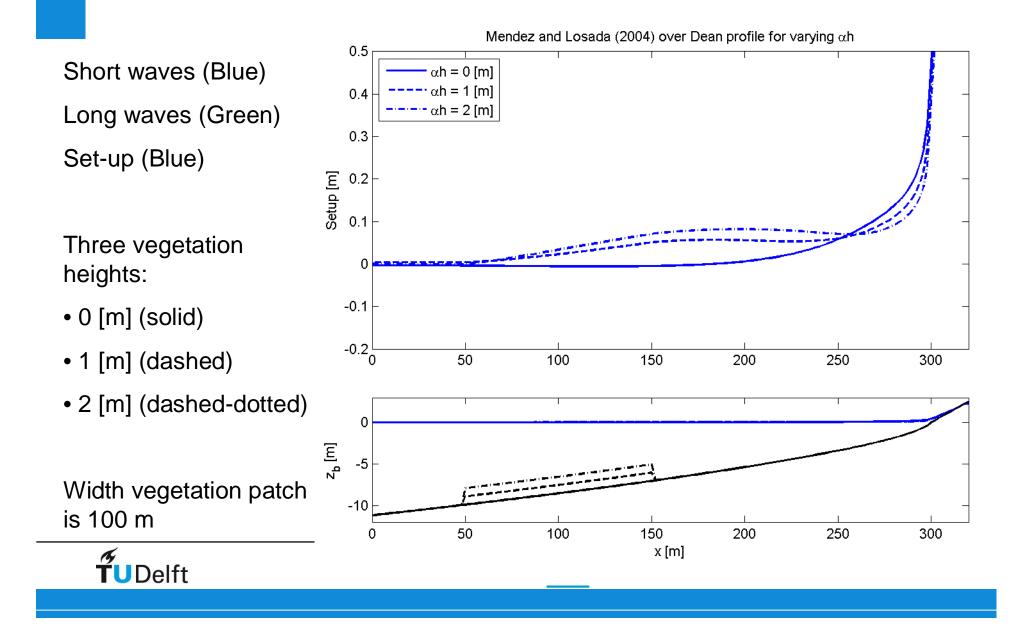




Breaking uni-directional waves



Breaking uni-directional waves (Stationary)



Next steps

Include cohesive fractions

Compare to field observations

 Work on wave set-up in vegetation fields

 Explore erosion meganism (PhD Student Linh Phan Khanh









Part II

Non-hydrostatic model and ground water flow:

- Gravel beaches







Gravel beaches, PhD work Robert McCall

- Gravel beaches occur in many high-lattitude areas around the world (Northern Europe, Russia, North America, Australia & NZ, Argentina and Chile)
- Considered sustainable forms of coastal defence due to ability to absorb large amounts of wave energy
- Little knowledge of processes occurring on gravel beaches, particularly during storms
- Few (if any) tools available to coastal managers of gravel beaches to assess flood risk







Gravel beaches differ from sandy beaches:

	Sand	Gravel
Waves	Large dissipative surf zone	Waves break at shoreline,
	Dominance of infragravity waves at shoreline	Incident band and iG energy at shoreline

	Sand	Gravel
Groundwater	Low infiltration rates,	High infiltration rates, leading to large swash asymmetry and onshore transport
	Groundwater level unimportant	Groundwater level can influence zones and magnitudes of erosion and deposition







Gravel beaches differ from sandy beaches:

	Sand	Gravel
Sediment transport	in surf zone and swash	swash zone
	Suspended transport	Bed load and sheet flow
	Limited effect of grain interactions	Large spread in grain size leads to exposure and hiding effects. Saltation of casts

	Sand	Gravel
Morphology	Time scale of storm and response similar	Time scale of response (~minutes) shorter than storm.
	beach flattening	often beach steepening
۶ U	High energy event leads to longshore uniform morphology	High energy event may increase or develop longshore rhythmicity

Model development

- Development of groundwater model to account for infiltration and exfiltration on gravel beaches
 - ✓ Completed. Results presented McCall et al, ICCE 2012
- Validation of phase-resolving wave model (similar to TUDelft SWASH model) for steep, reflective gravel beaches
 ✓ Almost complete. McCall et al. Journal publication in prep.
- Development of gravel sediment transport and morphology processes in XBeach
 - **x** To be done 2013-2014
- Development of practical coastal management tools
 ✓ First steps taken. Presented at McCall et al., ICS 2013



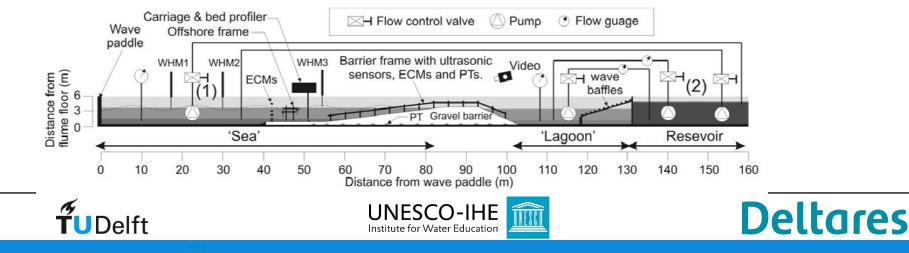


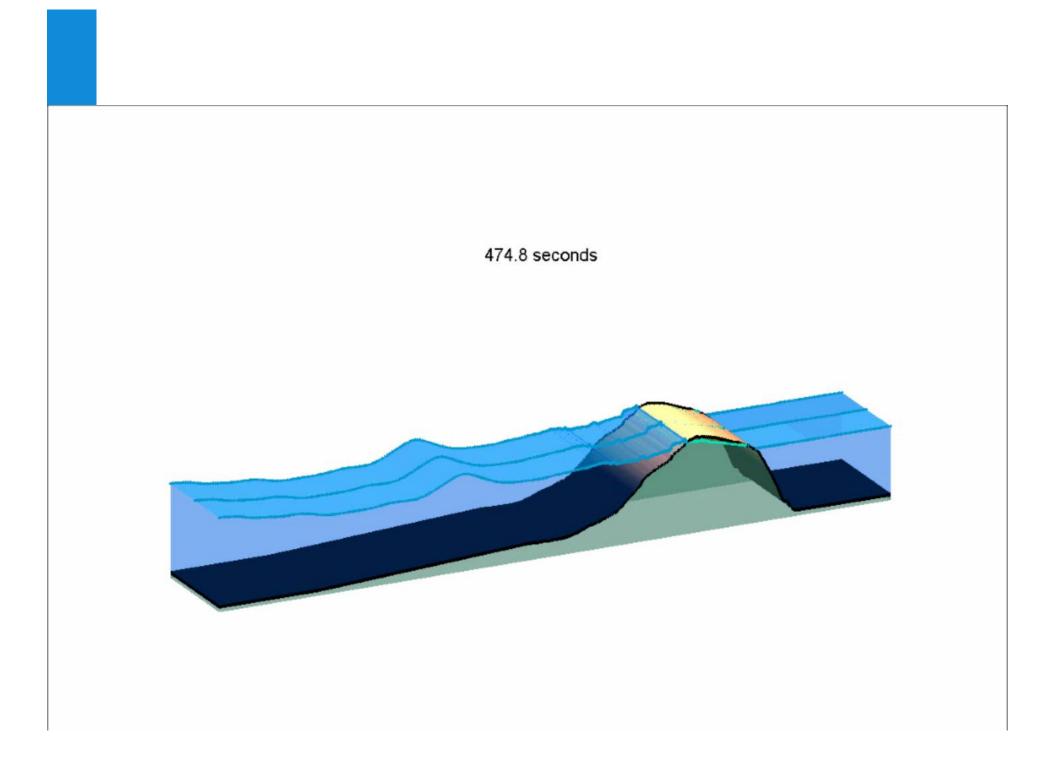


Model validation

- Gravel barrier dynamics experiment in Delta Flume (BARDEX, Hydralab)
- 4m high, 50 m wide permeable gravel barrier
- Varying wave conditions and water levels
- Large dataset of swash and overwash hydrodynamics and morphodynamics

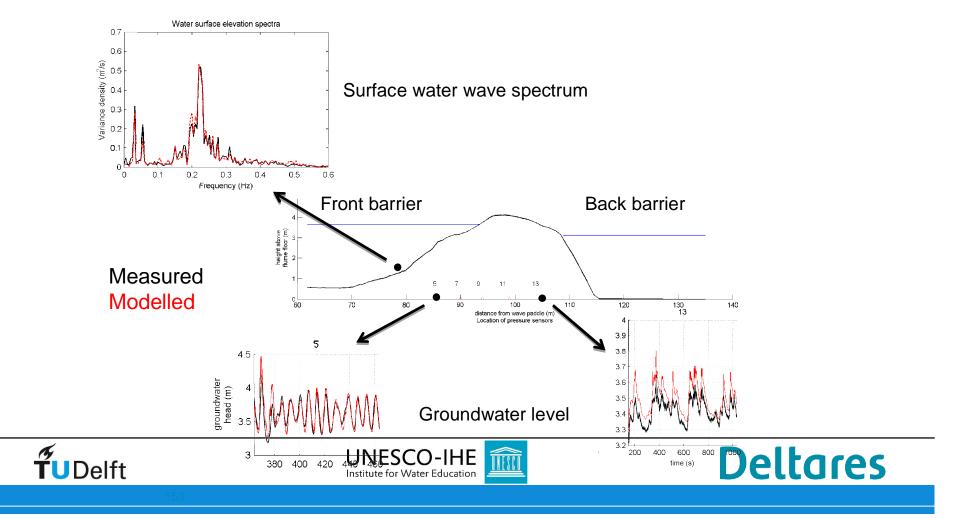






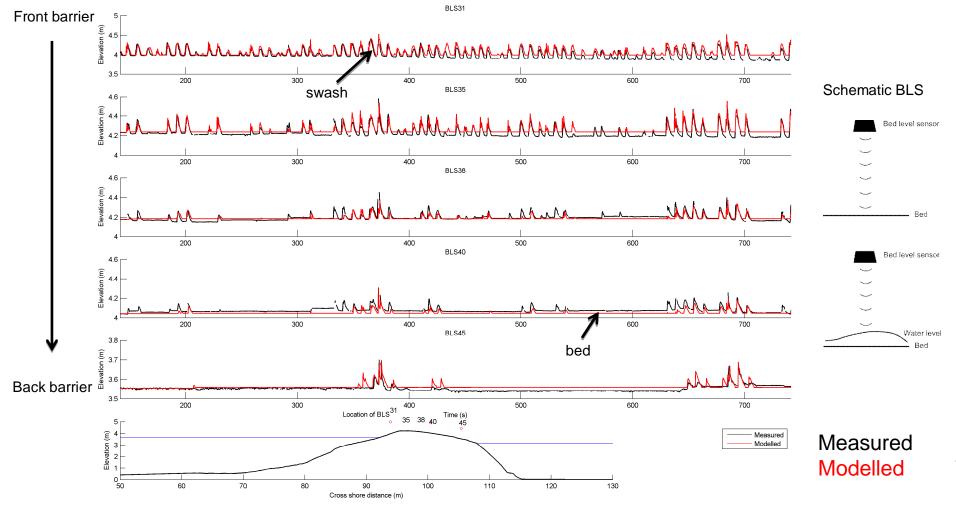
Model validation

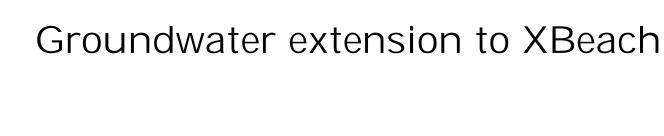
- Good reproduction of groundwater level variations
- Transformation of waves towards gravel barrier modelled well



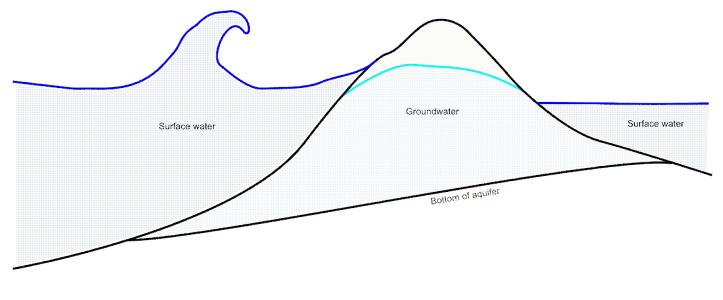
Model validation

- Very good reproduction of overwash events
- Inclusion of infiltration essential in correct modelling of overwash





• Separate surface water regime and groundwater regime



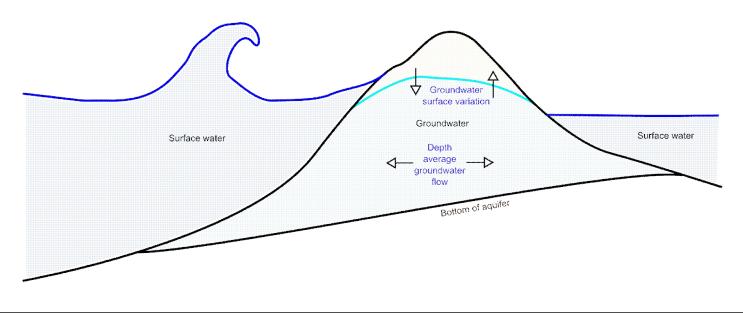






Groundwater extension to XBeach

- Separate surface water regime and groundwater regime
- Darcy-type depth average horizontal groundwater flow



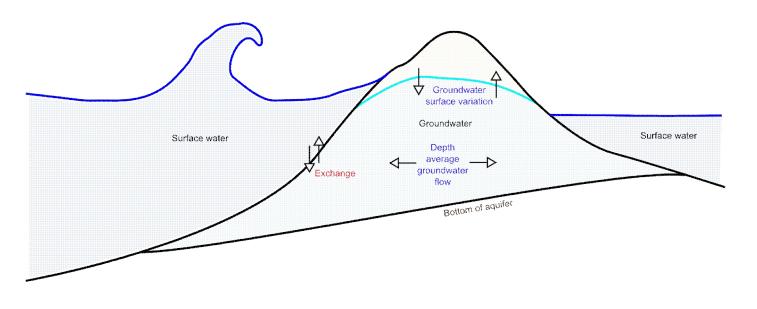






Groundwater extension to XBeach

- Separate surface water regime and groundwater regime
- Darcy-type depth average horizontal groundwater flow
- Vertical exchange of water using estimate of vertical head gradient



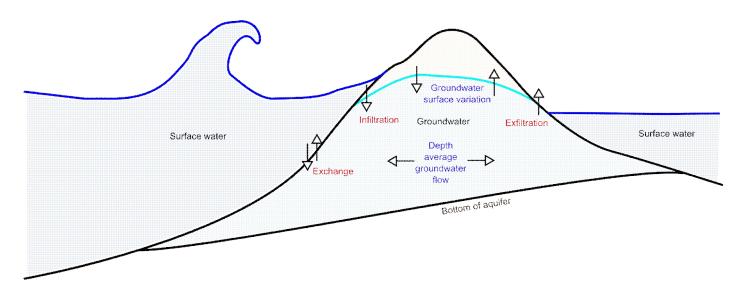




Deltares

Groundwater extension to XBeach

- Separate surface water regime and groundwater regime
- Darcy-type depth average horizontal groundwater flow
- Vertical exchange of water using estimate of vertical head gradient
- Infiltration and exfiltration where regimes are unconnected



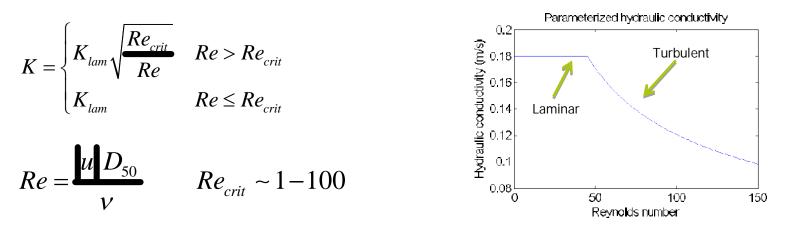






Central equations

- Continuity $\nabla \vec{U} = 0$ $\vec{U} = \begin{bmatrix} u \\ w \end{bmatrix}$ • Equation of motion $K\nabla H + \vec{U} = 0$ $H = z + \frac{p}{\rho g}$
- Parametric inclusion of turbulent groundwater flow (Kuniansky et al., 2008; Shoemaker et al., 2008)



Deltares





Non-hydrostatic equations in XBeach

• 1D equations:

$$\begin{split} \frac{\delta\zeta}{\delta t} + \frac{\delta hu}{\delta x} + S &= 0 \\ \frac{\delta u}{\delta t} + u \frac{\delta u}{\delta x} - \upsilon_h \frac{\delta^2 u}{\delta x^2} = -\frac{1}{\rho} \frac{\delta \left(\bar{q} + \rho g \zeta\right)}{\delta x} - c_f \frac{u \left|u\right|}{h} \end{split}$$







Non-hydrostatic model (2)

Waves model input (described in draft nonhydrostatic report):

- Use XBeach nonhydrostatic model
 - parameter 'nonh' turns on nonhydrostatic pressure correction
- Wave boundary conditions for nonhydrostatic model
 - parameter 'wbcversion = 3' uses the most advanced wave boundary condition generation scheme
 - parameter 'nonhspectrum = 1' sets XBeach to generate individual random waves from a spectrum
 - parameter 'instat' sets the type of spectrum file to be read (parameterised, SWAN, or 2D variance density table)
 - parameter 'front = nonh_1d' sets the offshore boundary condition to (1D) absorbing/generating for nonhydrostatic wave simulations
 - other parameters can be the same as described in the XBeach manual







Non-hydrostatic model (3)

Waves model input (described in draft nonhydrostatic report):

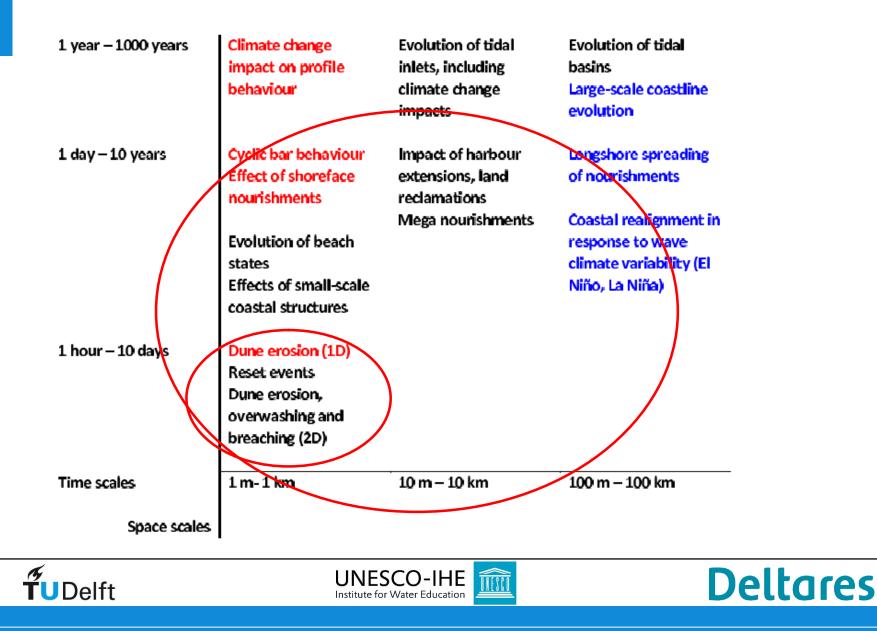
- Numerical parameters
 - parameter 'solver=2' uses a fast nonhydrostatic pressure solver that can only be used in 1D simulations, else use slower 'solver=1'
 - set parameter 'Topt' to the dominant wave period in your simulation



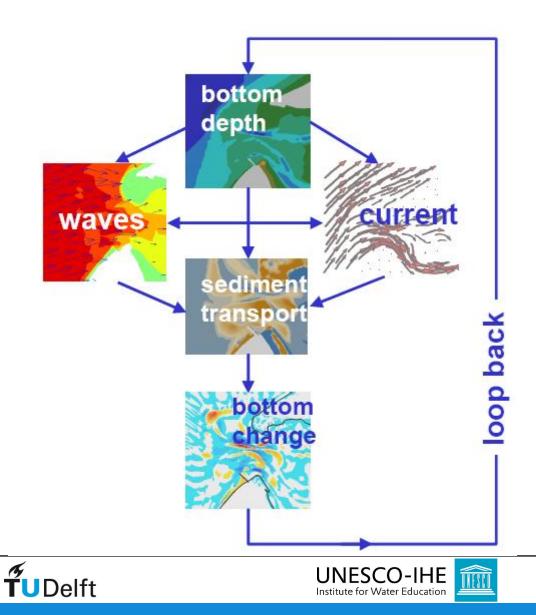




Long term stationary solutions



Morphodynamic loop



- Bottom changes are fed back into bathymetry after each time step
- Bottom changes are multiplied by morphological factor MORFAC
- Difference between hydrodynamic time scale and morphodynamic timescale



Morfac options

- We can either:
 - Specify morphological time and adjust hydrodynamic time, or
 - Specify hydrodynamic time and adjust morphological time
- In the first option (morfacopt=1):
 - All input times are divided by morfac
 - Time series of boundary conditions are shortened
 - Tidal dynamics may be distorted
 - Time series of wave energy may get too short
- In the second option (morfacopt=0):
 - Hydrodynamic time series are untouched
 - Tidal dynamics are preserved
 - Effects of changes within tidal cycle are exaggerated









Morfacopt

Options for using morfac:

Morfacopt=0	Morfacopt=1 (default)
Times are specified as hydrodynamic times	Times are specified as morphological times
Hydrodynamics of tidal cycle are not disturbed	All times divided by Morfac Tidal variation is accelerated







Differences in approach / Considerations

- Need to calibrate longer-term profile behavior
- More attention to onshore processes
 - facua or facsk, facas
- During moderate conditions, infragravity waves much less important
- Stationary approach possible if infragravity waves can be neglected
- Higher morphological factor for moderate conditions

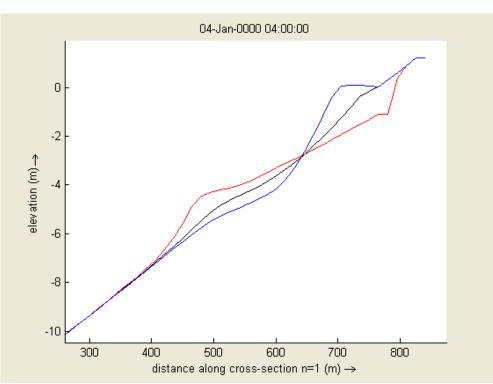






Example profile evolution

- River outflow case turned into 1D model of straight beach, to calibrate profile behaviour
- Facua (=facsk=facas)= 0.0, 0.2,0.4
- Which is which?
- More subtle calibration is possible using separate values for facas and facsk
- facas effects shoreline
- facsk effects surfzone



Deltares





Stationary wave solver

• First, the wave and roller balances are iterated per longshore line until no change; screen output tells how many iterations

Short waves
And
Rollers

$$\frac{\partial A}{\partial t} + \frac{\partial c_x A}{\partial x} + \frac{\partial c_y A}{\partial y} + \frac{\partial c_\theta A}{\partial \theta} = -\frac{D_w}{\sigma}$$

$$\frac{\partial S_r}{\partial t} + \frac{\partial c_x S_r}{\partial x} + \frac{\partial c_y S_r}{\partial y} + \frac{\partial c_\theta S_r}{\partial \theta} = -D_r + D_w$$

• Then wave and roller forces are computed

$$F_{x} = -\left(\frac{\partial S_{xx}}{\partial x} + \frac{\partial S_{xy}}{\partial y}\right)$$
$$F_{y} = -\left(\frac{\partial S_{xy}}{\partial x} + \frac{\partial S_{yy}}{\partial y}\right)$$

- NO WAVE GROUP FORCING
- Stationary run repeated every *wavint* seconds







Running stationary waves

- Instat = stat or stat_table
- Break = 2
 - Baldock formulations meant for wave-averaged simulations, other formulations meant for simulations varying on wave group scale
- Hrms =
 - Watch out: Hrms not Hm0
- Trep =
 - Representative period = Tp
- Dir0 =
 - Mean wave angle (nautical convention)
- Wavint = <interval of repeating wave simulation (s)>
 - Note: take into account morfac!







Presentation of local problems

by participants







Challenge the future